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A NEW FALLOUT TRANSPORT CODE FOR THE  
DELFIC SYSTEM: THE DIFFUSIVE TRANSPORT  
MODULE. SUPPLEMENT

Hillyer G. Norment

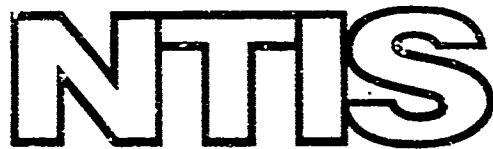
Mount Auburn Research Associates, Incorporated

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October 1972

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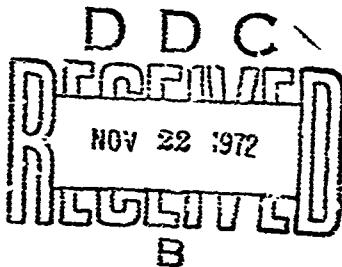
MT. AUBURN RESEARCH ASSOCIATES, INC.  
385 Elliot Street  
Newton, Massachusetts 02164

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## ABSTRACT

The Diffusive Transport Module of the new DELFIC fall-out prediction system has undergone additional development since publication of its description in DASA 2669. This supplement to DASA 2669 describes these developments and presents amendments and corrections to the code and its documentation. Complete FORTRAN statement listings of subroutines that have been substantially changed are included.

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## 1. INTRODUCTION

Since publication of DASA 2669\*, development and application of the DELFIC Diffusive Transport Module (DTM) has continued. A few revisions to the model have been made, several of them of major importance. In addition, some hidden "bugs" have been uncovered and corrected. In this supplement to DASA 2669 we describe the important model revisions, and amend the documentation. We also correct errors in the documentation, and provide FORTRAN statement listings of subroutines that have been changed substantially.

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\* H. G. Norment and E. J. Tichovolsky, "A New Fallout Transport Code for the DELFIC System: The Diffusive Transport Module," ARCON Corporation Report R71-1W, DASA 2669 (1 March 1971), AD 727 613.

## 2. MODEL REVISIONS

### 2.1 Initial Parcel Description

Fallout parcels are taken to be distributed in the horizontal about their centers of mass by a Gaussian density function. The initial Gaussian standard deviation was set equal to the parcel radius that was received via tape IPARIN from the Cloud Rise-Transport Interface Module. This has been changed so that the initial standard deviation is one-half the input parcel radius. (Compare subroutine SPRVS card 81 of DASA 2669 with SPRVS card 94 of this supplement.)

### 2.2 Simple Advection-Plus-Settling

In some cases, it is desirable to transport fallout in a simple advection-plus-settling mode; that is, without accounting for diffusion in the vertical. In this mode, integration of Eq. (16) is bypassed, and the parcel trajectory is computed via Eq. (32). As actually employed in the original DTM, Eq. (32) was modified to the form

$$\vec{r}_c = \vec{r}_i + \frac{1}{\langle f \rangle - \langle w \rangle} \sum_{z_j}^{z_g} \vec{U}(x, y, z, t) \Delta z ,$$

where the average settling speed,  $\langle f \rangle$ , was taken to be

$$\langle f \rangle = \frac{f(z_i) + f(z_g)}{2}$$

and  $\langle w \rangle$  was an average vertical air velocity. For cases where  $z_i - z_g$  is large, there can be significant differences in the particle settling speeds in the upper layers compared with those in the lower layers. When, in addition, there is large wind shear in the vertical,

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it becomes necessary to use settling speeds that are computed individually for each wind layer instead of an average settling speed. The code has been changed so that this is done.

Major changes have been required in several programs. The most extensive changes are in subroutines SPRVS and TRANP. A new array, CAVS(KBHF), is created to store a table of particle settling speeds; it contains an entry for each wind layer.

Before a parcel is transported via this mode, a test is made to determine if the parcel can impact in the time allowed for transport. This test is simplified by using the knowledge that all parcels comprised of particles of a particular size class are processed sequentially in one group. Thus, as each new particle size class is encountered, the altitude above which these particles cannot impact is computed. Then, any parcel in the group whose base is above this altitude is bypassed. To perform the altitude limit calculation, an average vertical wind velocity is needed for each wind layer. To accommodate this, the array WAVG(LTIME) was changed to the array WAVG(KBHF,LTIME).

### 3. DOCUMENTATION REVISIONS

Revisions and corrections are intermixed and listed in order of their encounter in DASA 2669.

Page 27, Eq. (23):

$$t_1 = 4c_3 \left( \frac{\sigma_{t_i}^2}{\epsilon} \right)^{1/3} \quad (23)$$

Page 27, line 16:

In our application,  $\sigma_{t_i}$  is taken to be one-half of the radius of a cloud wafer as recorded

Page 44, line 3:

where the summation is over the N data with the largest  $f_i$ , and the weighting factors,

Page 44, lines 6 and 7:

The parameters  $\alpha$ ,  $\beta$ , and  $N$  are specified by the user and the  $x_i$  and  $y_i$  are relative to the n-th lattice cell center. The calculations of the  $f_i$  are performed so that whenever a factor in Eq. (39) is found to

Page 44, lines 9 and 10:

than the total number of observations,  $M$ , only the  $N$  observations with the largest  $f_i$  relative to the n-th lattice cell center are considered in the calculations.

Page 45, lines 8-12:

list, two tables of settling rates for this particle are computed. One table contains an entry for each altitude increment used in the numerical integration of Eq. (16).

The other table contains an entry for each of the larger altitude increments that are used to resolve the wind and turbulence fields. These same tables are used through transport for this parcel and the remainder of the parcels in the first group. When the first parcel of the second group is selected, new tables are computed, and so on.

Page 49, Eq. (45):

$$\frac{G_j^{n+1} - G_j^n}{\Delta t} = \frac{1}{2(\Delta z)^2} \left[ (K_{j+1} + K_j) G_{j+1}^n - (K_{j+1} + 2K_j + K_{j-1}) G_j^n + (K_j + K_{j-1}) G_{j-1}^n \right] + \frac{1}{\Delta z} \left[ (f_{j+1} - w_{j+1}) G_{j+1}^n - (f_j - w_j) G_j^n \right] \quad (45)$$

Page 53, following Eq. (65):

where in the code  $K_{j+1}$  is taken to be equal to  $K_j$ .

Page 66, paragraphs 1 and 2:

Beginning at its input location and time, the parcel base or top is transported via local winds in the cell of its residence. At the same time it settles at a speed that is computed for the altitude at the center of the wind cell of its residence. When it passes through a wind cell boundary or a time boundary, the wind and settling speed are changed to those of the new cell or update. This continues until ground impaction occurs or until an extreme wind field or time boundary is encountered. The calculation requires one step for each cell through which the base or top passes.

When an extreme boundary is encountered by a top or base, the location and time of the encounter is recorded. These values are used in the definition of the deposit increment as described on page 70. The altitude of a deposit increment is always recorded as the arithmetic average of the impact

altitudes of its top and base. Thus, the recorded altitude of a deposit increment that has reached an extreme boundary can be well above the deposition plane.

Page 71, Figure 9:

The quantity labeled  $\sigma(\perp)$  that lies to the left of the deposit increment ellipse should be replaced by  $\sigma(\perp)_d$ .

Page 88, lines 10 and 11:

DFZ. An area-weighted average vertical wind, WAVG(KBH,LTIM), is derived from array WFZ for each altitude layer and update. Likewise, a volume-weighted

Page 88, equation for DKAV:

$$DKAV = \sum_{KBH=1}^{KBHX-1} \frac{DFZ(KBH, NDATA, LTIM) * (ZBH(KBH+1) - ZBH(KBH))}{ZBH(KBH) - ZBH(1)}$$

Page 88, lines 27 and 28:

out on ISOOUT. In a parallel operation the quantities WAVG(KBH,LTIM), which are area-weighted vertical wind velocities for each wind layer and update, are computed and printed out on

Page 96, line 25:

in the horizontal RWFR(J)/2.0;

page 97, line 12:

ZPAR(J), PSAM(J), RWFR(J)/2.0, DWFR(J), ZLWF(J), and VWFR(J) are

Page 98, line 2:

for further details.) Also computed are the settling speeds,

CAVS(KBH), for each altitude, and the altitude, ZLIM, above which deposition is impossible, via gravity settling in the specified wind field, for particles in the particular size class being considered.

Page 100, last line:

CAV ← CAV - WAVGK

Page 101, first line:

WAVGK and DAVG(1) are the average vertical components of wind

Page 101, line 15:

ground by advection at fall rates CAVS(KBHF) via a call to subroutine ADVEC.

Page 101, line 23:

limit: i.e., whenever  $ZLCW \geq ZLIM$ . The comment

Page 110, lines 16-19:

also obtained via the COMMON area QPARM. The particle settling speeds, CAVS(KBHF), and area-weighted vertical air velocities, WAVG(KBHF,LTIMF), for each wind layer, are obtained

Page 110, line 27:

parcel base is advected, while settling at speeds CAVS(KBH) - WAVG(KBH,LTIM), from position  $(XP, YP, ZP =$

Page 110, line 29:

TOL. The standard deviations of the

Page 110, line 33:

parcel top is advected, while settling at speeds CAVS(KBH) -  
WAVG(KBH,LTIM), from position (XP,YF,

Page 111, line 2:

at time TQU. The standard

Page 111, second paragraph:

After both base and top of a parcel have been transported, the arithmetic average of the two impact times and impact altitudes are recorded for the deposit increment (as shown on the next page). In the event that the base or top encounters an extreme wind field or time boundary during transport, subroutine TRANP returns the coordinates of the encounter point. Therefore, the altitude recorded for a deposit increment can be well above the deposition plane.

Page 111, third paragraph, lines 4 and 5:

is considered superfluous whenever ZP differs from ZDEP by less than 0.1. Instead, XOL, YOL, ZOL, TCL, SIGXI, SIGYL,

Page 122, line 28:

When vertical diffusive transport is employed, the computation of horizontal parcel advection is based on the

Page 123, insert between the second and third paragraphs:

For transport via simple advection plus settling, TRANP is called by subroutine ADVEC with KRP=0 (otherwise KRP=1). The parcel top or bottom is transported stepwise through the vertical layers between ZP and ZDEP via the layerwise mode (see below). In each layer, with index KBH, the vertical velocity is

WBAR = WFZ(KBH, NDATO, ..TIM) - CAVS(KBH)

and KAY = - .i. TSEG is computed as shown by the equation in the preceding paragraph.

Page 123, third paragraph, line 3:

is traversed at a time. This mode is mandatory for transport via simple advection plus settling, or when a parcel trajectory

Page 125, line 6:

The rapid computation mode is employed for vertical diffusive transport when

Page 145, insert at the end of the Input Data Card 4 discussion:

To preempt vertical diffusive transport, set KX=1 and set ZMAX arbitrarily large. This causes all parcels to be transported via the simple-advection-plus-settling mode (Eq. (32)). Of course, horizontal diffusive growth of parcels is accounted for in any case.

Page 146, line 14:

CSKIP = 0.1

Page 152, line 8:

HITIME. If the vertical diffusive mode of transport is used, the KBHX<sup>th</sup> base should be above or at the top of the transport space as this top is specified by ZMAX.

Page 156, Table 4, Record Number 12, Line 6 under Content:

size class central diameter ( $\mu\text{m}$ ), mass of fallout (kg)

Page 154, to the end of paragraph 1 add:

However, the turbulent energy dissipation rates can be input only for the horizontal directions; for the vertical direction Fickian diffusivities always are input, regardless of which type of data are input for the horizontal.

#### 4. CODE REVISIONS

##### 4.1 Single Card Changes

Addition of the arrays CAVS(KSHF) and WAVG(KSHF,LTIMF) requires revisions in DIMENSION statements and subroutine argument lists. However, complete FORTRAN statement listings are given in this supplement for all subroutines that require these revisions.

Subroutine EOUN, card 27:

```
CALL NEST (NET, NETSU, X0, Y0, NDATO, XL, XR, YL, YU, ICF,  
          JCF, NCF)
```

Subroutine DUMPER:

Place card 33 in its proper position.

Subroutine NEST, insert between cards 20 and 21:

```
DIMENSION NET(ICF, JCF), NETSU(NCF)
```

##### 4.2 FORTRAN Statement Listings

Complete FORTRAN statement listings are given for the following subroutines. These subroutines are operational on the UNIVAC 1108.

<u>Subroutine</u>	<u>Page</u>
C31M	13
ADMIN	18
ADVEC	21
AMBNT	23
SPRVS	26
TRANP	32

The machine used to prepare these listings prints a # symbol to represent a 4-8 punch; this symbol should be an apostrophe (''). In FORMAT and DATA statements, the apostrophe is used to define Hollerith character fields.

SEPTEMBER 1971	C31M	1
C31M IS THE MAIN PROGRAM WHICH DIRECTS THE DIFFUSIVE TRANSPORT	C31M	2
MODULE OPERATIONS. THE OBJECT-TIME DIMENSIONS ARE SET IN C31M.	C31M	3
THESE DIMENSIONS AND THEIR RESPECTIVE ARRAYS ARE	C31M	4
KKF - AA,BB,CC,DENUM,E,F,Q,H,DIFF,ZHT	C31M	5
LTMIF - TIMUP,DAVG,WAVG	C31M	6
KBHF - ZBH,ZCH	C31M	7
NDATEF - KTOPO	C31M	8
KBHF, NDATEF, LTMIF - DFZ,DXSUM,DYSUM,USUM,VSUM,WFZ,RSUM	C31M	9
ICF, JCF - NET	C31M	10
NCF - NETSU	C31M	11
MARF - MARY	C31M	12
NATF - ALT,ATEMP,RHO	C31M	13
DATA LITERALS MUST BE INSERTED IN THE DIMENSION STATEMENTS AND IN	C31M	14
THE RIGHT HAND SIDES OF THE ARITHMETIC STATEMENTS IN WHICH THE	C31M	15
ABOVE VARIABLE NAMES APPEAR.	C31M	16
***** GLOSSARY *****	C31M	17
AA(K) - EQUALS S2*(CJFF(K+1)+DIFF(K))+S1*F(K+1)	C31M	18
ALT - ALTITUDES FOR ATMOS. DENSITY AND VISCOSITY TABLE	C31M	19
ATEMP - DYNAMIC VISCOSITY OF AIR DATA VECTOR FOR ATMOS. TABLE	C31M	20
BB(K) - EQUALS S2*(CJFF(K+1)+2.*DIFF(K)+DIFF(K-1))+S1*F(K)	C31M	21
CAV - AVG. FALLRATE USED IN COMPUTING PDEST. IT APPLIES MID WAY	C31M	22
FROM PARCEL TOF TO ZMIN.	C31M	23
CAVS - PARTICLE FALL RATE FOR EACH ATMOS. STRATUM	C31M	24
CC(K) - EQUALS S1*(CJFF(K)+DIFF(K-1))	C31M	25
CROSS - CROSSWIND CROSSING TRAJECTORIES CORRECTION TO TURB.	C31M	26
CSKIP - TOTAL FRACTIONAL PARCEL DEPOSITION THRESHOLD	C31M	27
DAVG - AVG. ATMOS. VERT. TURB. PER UPDATE DATA VECTOR	C31M	28
DENCM(K) - EQUALS 1.-THETA*(BB(K)-CC(K)*E(K-1))	C31M	29
DEP - DEPOSITED FRACTIONAL MASS INCREMENT	C31M	30
DIFF(K) - VERT. DIFFUSIVITY AT K-TH SMALL ALTITUDE INCREMENT	C31M	31
DFKXS1 - VERTICAL DIFFUSIVITY AT ALTITUDE INCREMENT KX-1	C31M	32
DFZ - TURBULENCE Z COMPONENT 3-DIM. DATA ARRAY	C31M	33
DTNCR - RATE OF CHANGE OF FRACTIONAL MASS DEPOS. RATE THRESH.	C31M	34
DOPEN - MASS DEPOSITION RATE THRESHOLD	C31M	35
DOWN - DOWNWIND CROSSING TRAJECTORIES CORRECTION TO TURB.	C31M	36
DT - SMALL ITERATION TIME STEP FOR VERT. DIFF. DIFF. EQ.	C31M	37
DHAF - PARCEL VERT. THICKNESS BEFORE ADVECTION	C31M	38
DXSUM - TURBULENCE X COMPONENT (WEIGHTED SUM) 3-DIM. DATA ARRAY	C31M	39
DYSUM - TURBULENCE Y COMPONENT (WEIGHTED SUM) 3-DIM. DATA ARRAY	C31M	40
DZ - SMALL ALTITUDE INCREMENT FOR VERT. DIFF. DIFF. EQ.	C31M	41
DZMIN - MINIMUM VALUE OF DZ	C31M	42
E(K) - EQUALS THETA*AA(K)/DENCM(K)	C31M	43
EDDY - RATIO OF LAGRANGIAN TURBULENCE TIME SCALE TO EULERIAN	C31M	44
TURBULENCE LENGTH SCALE	C31M	45
EFFLUX - UPPER EFFLUX FRACTIONAL MASS	C31M	46
F(K) - IN SUB. DIFFE, WORKING SPACE IMPLICIT METHOD DATA VECTOR.	C31M	47
IN SUB. AMBNT, WORKING SPACE FOR VERTICAL VELOCITIES	C31M	48
FAV - MID-ATMOS. AVG. FALLRATE. USED IN CROSSING TRAJECTORIES	C31M	49
CORRECTIONS AND IN TRUNCATION ERROR ESTIMATION .	C31M	50
FMAB - CUMULATIVE FRACTIONAL MASS AIRBORNE	C31M	51
FMBEL - MIN. PARCEL FRACTIONAL MASS ALOFT TO BE TRANSPORTED	C31M	52
ICF - MAX. FORMAL DIM. CORRESPONDING TO ICX	C31M	53
IX - OBJECT-TIME FIRST MAX. DIM. OF ARRAY NET. NUMBER OF NET	C31M	54
MESSES IN EAST-WEST ROW.	C31M	55
IOPRIN - LOGICAL UNIT NUMBER OF CR-TRANS. INTER. MOD. OUTPUT TAPE	C31M	56
IPOUT - LOGICAL UNIT NUMBER OF DIFF. TRANS. MOD. OUTPUT TAPE	C31M	57
ISIN - LOGICAL UNIT NUMBER OF SYSTEM INPUT TAPE	C31M	58

C	ISOUT - LOGICAL UNIT NUMBER OF SYSTEM OUTPUT TAPE	C31M	59
C	JCF - MAX. FORMAL DIM. CORRESPONDING TO JCX	C31M	60
C	JCX - OBJECT-TIME SECOND MAX. DIM. OF ARRAY NET. NUMBER OF NET MESHES IN SOUTH-NORTH ROW.	C31M	61
C	KBH - ATMOS. VERT. SPACE INDEX FOR ARRAYS USUM,VSUM,WFZ,DXSUM, DYSUM, DFZ, RSUM, ZBH, ZCH	C31M	62
C	KBHF - MAX. FORMAL DIM. CORRESPONDING TO KBHX	C31M	64
C	KBHX - OBJECT-TIME MAX. VALUE OF KBH	C31M	65
C	KKF - MAX. FORMAL DIM. CORRESPONDING TO KFX	C31M	66
C	KKM - ALWAYS EQUALS 2. CORRESPONDS TO K=0 ALTITUDE INCREMENT	C31M	67
C	KKMA1 - EQUALS KKM+1	C31M	68
C	KXX - EQUALS KX+KKM	C31M	69
C	KKXS1 - EQUALS KXX-1	C31M	70
C	K <sup>o</sup> IP - CONTROL VARIABLE 0 FOR ADVECTIVE TRANSPORT 1 FOR DIFFUSIVE TRANSPORT	C31M	71
C	KTOPO - NET MESH AND SUR-MESH TOPOGRAPHY TABLE DATA VECTOR	C31M	72
C	KX - MAX. NUMBER OF DZ ALTITUDE INCREMENTS	C31M	73
C	KXMIN - MIN. NUMBER OF DZ ALTITUDE INCREMENTS	C31M	74
C	LSTEP - NUMBER OF IMPLICIT METHOD ITERATIONS. TDELT=LSTEP*DT.	C31M	75
C	DYSUM, DFZ, RSUM, TIMUP, DAVG, WAVG	C31M	76
C	LTIM - ATMOS. UPDATE TIME INDEX FOR ARRAYS USUM,VSUM,WFZ,DXSUM,	C31M	77
C	LTIMX - OBJECT-TIME MAX. VALUE OF LTIM	C31M	78
C	LTIMF - MAX. FORMAL DIM. CORRESPONDING TO LTIMX	C31M	79
C	MARF - MAX. FORMAL DIM. CORRESPONDING TO MARX	C31M	80
C	MARX - OBJECT-TIME MAX. DIM. OF ARRAY MARY	C31M	81
C	MARY - HORIZ. ATMOS. SPACE RESOLUTION NET MESH AND SUB-MESH CONTROL FLAGS DATA VECTOR	C31M	82
C	MC - CONTROL INTEGER DATA VECTOR	C31M	83
C	MC(1) LESS THAN OR EQUAL TO ZERO, SUPPRESSES LISTING OF EXPANDED WIND AND TURB. DATA	C31M	84
C	MC(1) GREATER THAN OR EQUAL TO ONE, CAUSES LISTING OF WIND AND TURB. DATA BEFORE SUMMATION	C31M	85
C	MC(1) EQUALS TWO, CAUSES LISTING OF WIND AND TURB. DATA AFTER SUMMATION	C31M	86
C	MC(2) EQUALS ONE, SUPPRESSES LISTING OF ATMOS. VISC. AND DENS. TABLES	C31M	87
C	MC(3) EQUALS ZERO, SUPPRESSES LISTING OF DEPOSIT INCREMENTS ON TAPE ISOUT	C31M	88
C	MC(4) EQUALS ONE, CAUSES PRINTOUT OF TRANSPORT INTERMEDIATE RESULTS ON TAPE ISOUT. WARNING. PRINTOUT IS EXTRAORDINARILY VOLUMINOUS. FOR DEBUGGING ONLY.	C31M	89
C	MC(7) EQUALS ONE, SUPPRESSES LISTING OF RAW WIND AND TURB. INPUT DATA	C31M	90
C	MC(10) EQUALS ONE, CAUSES TURB. DATA TO BE TREATED AS KOLMOGOROFF-BACHELOR ENERGY DISSIPATION RATES	C31M	91
C	MC(10) NOT EQUAL TO ONE, CAUSES TURB. DATA TO BE TREATED AS FICKIAN DIFFUSIVITIES	C31M	92

	MC(18) EQUALS CNE, SUPPRESSES READING FROM TAPE Iparin AND WRITING CNTO TAPE Iput	C31M 117 C31M 118 C31M 119 C31M 120
MINT	- MIN. NUMBER OF DT SMALL TIME STEPS PER DEPOSIT INCREMENT TIME INTERVAL	C31M 121 C31M 122
NAT	- NUMBER OF ALTITUDE STRATA IN ATMOS. DENS. AND VISC. TABLE	C31M 123
NATF	- MAX. FORMAL DIM. CORRESPONDING TO NATE	C31M 124
NBLK	- RECORD BLOCK SIZE FOR DEPOSIT INCREMENT RECORDS	C31M 125
NCF	- MAX. FORMAL DIM. CORRESPONDING TO NCX	C31M 126
NCX	- OBJECT-TIME MAX. DIM. OF ARRAY NETSU	C31M 127
NDATA	- ATMOS. HORIZ. SPACE INDEX FOR ARRAYS USUM,VSUM,WFZ,DXSUM, DYSUM, DFZ, RSUM, KTOPo	C31M 128 C31M 129
NDATC	- HORIZONTAL INDEX OF LATTICE CELL CONTAINING POINT (XC,YC)	C31M 130
NDATO	- HORIZONTAL INDEX OF LATTICE CELL CONTAINING POINT (X0,Y0)	C31M 131
NDATP	- HORIZONTAL INDEX OF LATTICE CELL CONTAINING POINT (XP,YP)	C31M 132
NDATX	- OBJECT-TIME MAX. VALUE OF NDATA	C31M 133
NDATF	- MAX. FORMAL DIM. CORRESPONDING TO NDATA	C31M 134
NDELT	- NOMINAL NUMBER OF DEPOSIT INCREMENTS PER FALLOUT PARCEL	C31M 135
NET	- HORIZONTAL SPACE CONTROL NET MESH 2-DIM. ARRAY	C31M 136
NETSU	- HORIZONTAL SPACE CONTROL NET SUB-MESH DATA VECTOR	C31M 137
NSEQC	- STORAGE SEQUENCE ORDINAL OF FIRST PARCEL TO BE TRANSPORTED	C31M 138
PHI	- EQUALS 1-THETA	C31M 139
Q(K)	- CONCENTRATION IN K-TH ALTITUDE INCREMENT	C31M 140
RHO	- ATMOS. DENSITY DATA VECTOR FOR ATMOS. TABLE	C31M 141
RO	- WIND HEADING ORIENTATION ANGLE AFTER ADVECTION	C31M 142
ROPART	- FALLOUT PARTICLE DENSITY	C31M 143
RSUM	- WIND HEADING ORIENTATION ANGLE (WEIGHTED SUM) 3-DIM. ARRAY	C31M 144
RWAF	- PARCEL RADIAL IN PARCEL CENTRAL PLANE BEFORE ADVECTION	C31M 145
SIGX0	- PARCEL MASS HOR. STAND. DEV. DOWNWIND AFTER ADVECTION	C31M 146
SIGYC	- PARCEL MASS HOR. STAND. DEV. CROSSWIND AFTER ADVECTION	C31M 147
S1	- EQUALS DT/DZ	C31M 148
S2	- EQUALS DT/(2.*(DZ)**2)	C31M 149
TDELT	- CURRENT DEPOSIT INCREMENT TIME INTERVAL	C31M 150
TDEP	- ADVECTIVE TRANSPORT TIME INTERVAL	C31M 151
THFTA	- IMPLICIT FINITE DIFFERENCE PARAMETER	C31M 152
THETO	- DOUBLE PRECISION WORD CORRESPONDING TO THETA	C31M 153
TIME	- TIME AT ONSET OF CURRENT DEPOSIT INCREMENT TIME INTERVAL	C31M 154
TIMEX	- SIMULATED TRANSPORT TIME LIMIT	C31M 155
TIMUP	- ATMOSPHERE UPDATE TIMETABLE DATA VECTOR	C31M 156
TO	- TIME AFTER PARCEL ADVECTION	C31M 157
TP	- TIME BEFORE PARCEL ADVECTION	C31M 158
TPAUS	- TIME AT END OF CURRENT DEPOSIT INCREMENT TIME INTERVAL	C31M 159
USUM	- WIND X COMPONENT (WEIGHTED SUM) 3-DIM. DATA ARRAY	C31M 160
VETA	- VERTICAL DIFFUSION ABSORPTION COEFFICIENT	C31M 161
VSUM	- WIND Y COMPONENT (WEIGHTED SUM) 3-DIM. DATA ARRAY	C31M 162
W(K)	- SETTLING RATE AT K-TH SMALL ALTITUDE INCREMENT	C31M 163
WAVG	- AVG. ATMOS. VEKT. WIND PER UPDATE PER STRATUM	C31M 164
WAVGK	- WAVG AVERAGED OVER THE STRATA FOR THE FIRST UPDATE	C31M 165
WFZ	- WIND Z COMPONENT 3-DIM. DATA ARRAY	C31M 166
WINT	- NET CONTROL MESH DIMENSION	C31M 167
XLLC	- X COORDINATE OF SOUTH-WEST CORNER OF ATMOS. SPACE	C31M 168
X0	- PARCEL CENTER X COORDINATE AFTER ADVECTION	C31M 169
XP	- PARCEL CENTER X COORDINATE BEFORE ADVECTION	C31M 170
YLLC	- X COORDINATE OF SOUTH-WEST CORNER OF ATMOS. SPACE	C31M 171
Y0	- PARCEL CENTER Y COORDINATE AFTER ADVECTION	C31M 172
YP	- PARCEL CENTER Y COORDINATE BEFORE ADVECTION	C31M 173
ZBH	- ATMOSPHERE STRATA BASE-ALTITUDE DATA VECTOR	C31M 174

C	ZCH - ATMOSPHERE STRATA MID-ALTITUDE DATA VECTOR	C31M 175
C	ZDEP - ADVECTIVE TRANSPORT TERMINAL ALTITUDE	C31M 176
C	ZHT(K) - K-TH ALTITUDE INCREMENT ABOVE ZMIN LEVEL	C31M 177
C	ZLOW - PARCEL BASE ALTITUDE BEFORE ADVECTION	C31M 178
C	ZMAX - ATMOSPHERE TOP ALTITUDE (FOR VERT. DIFF. DIFF. EQ.)	C31M 179
C	ZMIN - GROUND LEVEL OR DEPOSITION PLANE ALTITUDE	C31M 180
L	ZO - PARCEL CENTER Z COORDINATE AFTER ADVECTION	C31M 181
C	ZP - PARCEL CENTER Z COORDINATE BEFORE ADVECTION, EXCEPT AS REDEFINED IN SUR. ADVEC	C31M 182
C	ZUPP - PARCEL TOP ALTITUDE BEFORE ADVECTION. ZLOW+DWAF	C31M 183
	DOUBLE PRECISION AA(204),BY(204),CC(204),CENDM(204),E(204),F(204)	C31M 185
	DOUBLE PRECISION D(204)	C31M 186
	DIMENSION ZBH( 27),ZCH( 27),TIMUP( 6),MARY( 1)	C31M 187
	UIMENSION KTOPO( 1),NETSU( 1),NET( 1, 1)	C31M 188
	DIMENSION DFZ( 27, 1, 6),WFZ( 27, 1, 6)	C31M 189
	DIMENSION USUM( 27, 1, 6),VSUM( 27, 1, 6)	C31M 190
	DIMENSION DXSUM( 27, 1, 6),DYSUM( 27, 1, 6)	C31M 191
	DIMENSION RSUM( 27, 1, 6),DAVG( 6)	C31M 192
	DIMENSION WAVG( 27, 6)	C31M 193
	DIMENSION ALT( 260),RHO( 260),ATEMP( 260)	C31M 194
	DIMENSION CAVS( 27),WI( 204),DIFF( 204),ZHT( 204)	C31M 195
	COMMON /QPARM/ IPOINT,IPARIN,NBLK ,NAT ,NDELT ,KX ,KKH	C31M 196
1	,NSEQO ,ICX ,JCX ,NCX ,KBHX ,NDATX ,LTIMX ,ISIN ,ISOUT	C31M 197
2	,EDDY ,FMREL ,LSPEF ,MC(13),WINT ,XLLC ,YLLC ,YHFTA ,ZMIN	C31M 198
3	,CSKIP ,MINT ,ZMAX ,TIMEX ,DT ,DZ ,XP ,YP ,ZP	C31M 199
4	,DINCR ,DOWN ,TP ,ZLOW ,DWAF ,PHAF ,ROPART,ZUPP ,VETA	C31M 200
5	,DOPEN ,CROSS ,TIME ,KKMA1 ,XXX ,KKS1 ,KXMIN ,NDATP	C31M 201
	ICF=1	C31M 202
	ISIN=5	C31M 203
	ISOUT=6	C31M 204
	IPARIN=9	C31M 205
	IPOINT=10	C31M 206
	JCF=1	C31M 207
	KBHF=27	C31M 208
	KKF=204	C31M 209
	LTIMF=6	C31M 210
	MARF=1	C31M 211
	NATF=260	C31M 212
	NCF=1	C31M 213
	NDATF=1	C31M 214
	DO 1 N=1,NCF	C31M 215
1	NETSU(N)=0	C31M 216
	DO 2 J=1,JCF	C31M 217
	DO 2 I=1,ICF	C31M 218
2	NET(I,J)=0	C31M 219
	DO 3 M=1,MARF	C31M 220
3	MARY(M)=0	C31M 221
	DO 4 K=1,KBHF	C31M 222
	ZBH(K)=0.	C31M 223
4	ZCH(K)=0.	C31M 224
	DO 104 K=1,KBHF	C31M 225
	DO 104 L=1,LTIMF	C31M 226
5	WAVG(K,L)=0.0	C31M 227
	DO 5 N=i,NDATF	C31M 228
5	KTOPO(N)=0	C31M 229
	DO 6 L=1,LTIMF	C31M 230
	TIMUP(L)=0.	C31M 231
	DAVG(L)=0.	C31M 232

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DO 6 N=1,N$ATF          C31M 233
DO 6 K=1,K$HF          C31M 234
DFZ(K,N,L)=0.          C31M 235
WFZ(K,N,L)=0.          C31M 236
USUM(K,N,L)=0.          C31M 237
VSUM(K,N,L)=0.          C31M 238
DXSUM(K,N,L)=0.          C31M 239
DYSUM(K,N,L)=0.          C31M 240
6 RSUM(K,N,L)=0.          C31M 241
COMMENCE READING DATA INPUTS FROM TAPES ISIN AND IPARIN      C31M 242
COMMENCE WRITING DATA OUTPUT HEADERS ONTO TAPES ISOUT AND IPUT      C31M 243
    CALL      LINK(ALT,RHO,ATEMP,NATF)          C31M 244
CONSTRUCT THE HORIZONTAL SPACE CONTROL NET          C31M 245
    CALL      GETUP(NET,NETSU,KTOPG,HARY,MARF,ICF,JCF,NCF,N$ATF)  C31M 246
CONSTRUCT THE ATMOSPHERIC STRATA AND UPDATE DATA VECTORS      C31M 247
    CALL      HITIMF(ZCH,ZRH,TIMUP,K$HF,LTIMF)          C31M 248
CONSTRUCT AND FILL IN THE ATMOSPHERIC LATTICE AND UPDATE STRUCTURE      C31M 249
    CALL      ADMIN(NET,NETSU,ZRH,ZCH,TIMUP,USUM,VSUM,DXSUM,DYSUM,  C31M 250
1RSUM,DFZ,WFZ,DAVG,WAVG,ICF,JCF,NCF,K$HF,N$ATF,LTIMF)          C31M 251
CIRCUMVENT ALL TAPE HANDLING IF MC(18) EQUALS 1          C31M 252
    IF(MC(18).EQ.1) GO TO 7          C31M 253
CALCULATE THE DIFFUSIVE TRANSPORT OF PARCELS ACCEPTED FROM TAPE IPARIN  C31M 254
COPY OUT RESULTS ONTO TAPE IPUT          C31M 255
    CALL      SPRVS(NET,NETSU,ZRH,ZCH,TIMUP,USUM,VSUM,DXSUM,DYSUM,  C31M 256
1RSUM,DFZ,WFZ,DAVG,WAVG,ALT,RHO,ATEMP,AA,BB,CC,DENOM,PIFF,E,F,Q,W,  C31M 257
2ZHT,ICF,JCF,NCF,K$HF,N$ATF,LTIMF,KKF,NATF,CAVS)          C31M 258
7 CALL EXIT          C31M 259
STOP          C31M 260
END          C31M 261

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SUBROUTINE ADMIN(NET,NETSU,ZBH,ZCH,TIMUP,USUM,VSUM,DXSUM,DYSUM,
1RSUM,DFZ,WFZ,DAVG,WAVG,ICF,JCF,NCF,KBHF,NDATF,LTIMF)
SEPTEMBER 1971

SURROUNTRINE ADMIN CONSTRUCTS WIND DATA ARRAYS
USUM, VSLM, WFZ, WAVG, RSUM
AND TURBULENCE DATA ARRAYS
DXSUM, DYSUM, DFZ, DAVG.
IN ADMIN ONLY LTIM AND SPEC ARE READ FROM TAPE ISIN.
SPEC - DATA SPECIES IDENTIFICATION WORD #WIND# OP #SPEC#
LTIM - UPDATE ORDINAL OF DATA SET. FIRST ATMOS. SET HAS LTIM=1.
SUB. MKDAT IS CALLED TO PERFORM DATA EXTRAPOLATIONS.
AREA - AREA OF HORIZ. SPACE NET
AREAN - AREA OF N-TF NET MESH OR SUB-MESH
COMMON /OPARM/ IPOINT,IPARIN,NBLK ,NAT ,NDELT ,KX ,KYM
1,NSEQJ ,JCX ,NCX ,KBHX ,NDATX ,LTIMX ,ISIN ,ISOUT
2,FRDY ,FMRFL ,LSTEP ,MC(18),WINT ,XLIC ,YLLC ,THETA ,ZMIN
3,CSKIP ,MINT ,ZMAX ,TIMEX ,DT ,DZ ,XP ,YP ,ZP
4,DTINC ,DOWN ,TP ,ZLOW ,DWAF ,RWAF ,ROPART,ZUPP ,VETA
5,OPEN ,CROSS ,TIME ,KKMA1 ,KXX ,KKXS1 ,KXMIN ,NDATP
DIMENSION RSUM(KBHF,NDATF,LTIMF),DAVG(LTIMF),WAVG(KBHF,LTIMF)
DIMENSION NET(ICF,JCF),NETSU(NCF),?CH(KBHF),TIMUP(LTIMF),ZBH(KBHF)
DIMENSION USUM(KBHF,NDATF,LTIMF),VSUM(KBHF,NDATF,LTIMF)
DIMENSION DXSUM(KBHF,NDATF,LTIMF),DYSUM(KBHF,NDATF,LTIMF)
DIMENSION DFZ(KBHF,NDATF,LTIMF),WFZ(KBHF,NDATF,LTIMF)
DIMENSION LW(10),LD(10)
INTEGER WIND,DFSN,DCNE,SPEC
DATA PROGRM/#ADMIN #
DATA WIND/#WIND#/
DATA DFSN/#DIFF#/
DATA DONE/#NO H#/FORMAT(#0#36X,#UPDATE TIME INDEX#I5,#. WIND GRID CELL INDEX#I5#) ADMIN 32
FORMAT(# WIND#2(6X,#HORIZONTAL#),6X,# VERTICAL #6X,#CROSSWIND #6X) ADMIN 33
1,# DOWNWIND #6X,# VERTICAL #6X,#HORIZONTAL#) ADMIN 34
FORMAT(# LAYER#6X,#E.-H. WIND#6X,#N.-S. WIND#6X,# WIND #3#6X,#ADMIN 35
2DIFFUSION #),6X,# ROTATION#) ADMIN 36
FORMAT(# INDEX#3(6X,# VELOCITY #),3(6X,# CONSTANT #),6X,# ANGLE#) ADMIN 37
FORMAT(# #I5,7E16.4) ADMIN 38
FORMAT(/25X,#WEIGHTED SUMS OVER ABOVE COLUMN ENTRIES#/) ADMIN 39
FORMAT(# #I5,2E16.4,16X,2E16.4,16X,E16.4) ADMIN 40
FORMAT(# #22X,#UPDATE#I4,#* CELL#I4, #* ADMIN 41
3AVG. VERT. DIFF. =#E12.4) ADMIN 42
FORMAT(36X,I2,8X,3A4) ADMIN 43
FORMAT(/25X,#ATMOSPHERE UPDATE#I4,# FOR TIMES LATER THAN #E12.4,# 1SECONDS#) ADMIN 44
FORMAT(# #25X,#* * * * * * * * * * * WINDFIELD EXTRAPOLATION * * * * * #ADMIN 46
1 * * * * #) ADMIN 47
FORMAT(# #25X,#* * * * * * * * * * * DIFFUSIVITY EXTRAPOLATION * * * * * #ADMIN 48
2 * * * * #) ADMIN 49
FORMAT(/25X,#UPDATE#I4,# OF THE WINDFIELD IS MISSING#) ADMIN 50
FORMAT(/25X,#UPDATE#I4,# OF THE DIFFUSIVITY IS MISSING#) ADMIN 51
FORMAT(# OVER ENTIRE HORIZONTAL GRID FOR UPDATE#T4, #* ADMIN 52
6 #* AVG. VERT. DIFF. =#E12.4) ADMIN 53
FORMAT(# AVG. VERT. VEL. FOR EACH STRATUM IS - #) ADMIN 54
FORMAT(2X,I5,E16.4) ADMIN 55
AREA=JCX*JCX*(WINT**2)
DO 999 L=1,LTIMX
LW(L)=L

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999 LD(L)=L                                ADMIN 59
COPY IN LTIM AND SPEC FROM TAPE ISIN AND CALL SUB. MKDAT   ADMIN 60
1000 READ(ISIN,9) LTIM,SPEC                ADMIN 61
      IF(SPEC.EQ.DCNE) GO TO 1301          ADMIN 62
      IF((LTIM.LT.1).OR.(LTIM.GT.LTIMX)) CALL ERROR(PROGRM,-1000,ISOUT)  ADMIN 63
      WRITE(ISOUT,10) LTIM,TIMUP(LTIM)      ADMIN 64
      IF(SPEC.EQ.WIND) GO TO 1101          ADMIN 65
      IF(SPEC.EQ.DFSN) GO TO 1201          ADMIN 66
      CALL ERROR(PROGRM,-1101,ISOUT)        ADMIN 67
1101 WRITE(ISOUT,11)                        ADMIN 68
      DO 1102 L=1,LTIMX                   ADMIN 69
1102 IF(LTIM.EQ.LW(L)) GC TO 1103        ADMIN 70
      CALL ERROR(PROGRM,-1102,ISOUT)        ADMIN 71
1103 LW(L)=-1                            ADMIN 72
      CALL      MKDAT(ZCF,NET,NETSU,LTIM, USUM, VSUM,WFZ,ICF,JCF,NCF,
      1KBHF,NDATF,LTIMF)                  ADMIN 73
      GO TO 1000                          ADMIN 74
1201 WRITE(ISOUT,12)                        ADMIN 75
      DO 1202 L=1,LTIMX                   ADMIN 76
1202 IF(LTIM.EQ.LD(L)) GC TO 1203        ADMIN 77
      CALL ERROR(PROGRM,-1202,ISOUT)        ADMIN 78
1203 LD(L)=-1                            ADMIN 79
      CALL      MKDAT(ZCF,NET,NETSU,LTIM,DXSUM,DYSUM,DFZ,ICF,JCF,NCF,
      1KBHF,NDATF,LTIMF)                  ADMIN 80
      GO TO 1000                          ADMIN 81
CHECK IF ANY WIND DATA SETS ARE MISSING    ADMIN 82
1301 DO 1303 L=1,LTIMX                   ADMIN 83
      IF(LW(L).EQ.-1) GO TO 1302          ADMIN 84
      WRITE(ISOUT,13) LTIM                ADMIN 85
      CALL ERROR(PROGRM,-1302,ISOUT)        ADMIN 86
CHECK IF ANY TURBULENCE DATA SETS ARE MISSING  ADMIN 87
1302 IF(LD(L).EQ.-1) GO TO 1303          ADMIN 88
      WRITE(ISOUT,14) LTIM                ADMIN 89
      CALL ERROR(PROGRM,-1303,ISOUT)        ADMIN 90
1303 CONTINUE                           ADMIN 91
CALCULATE THE WEIGHTED SUMS OVER ATMOS. STRATA AND REWRITE ARRAYS
C   USUM, VSUM, RSUM, DXSYM, DYSUM. ALSO COMPUTE DAVG AND WAVG.
ZSPAN=ZBH(KBHX)-ZBH(1)                    ADMIN 92
DO 922 L=1,LTIMX                         ADMIN 93
DO 1304 LK=1,KBHX                         ADMIN 94
1304 WAVG(LK,L)=0.0.                      ADMIN 95
DAVG(L)=0.                                ADMIN 96
DO 921 N=1,NDATX                         ADMIN 97
DKAV=0.                                    ADMIN 98
IF(MC(1).LT.1) GO TO 915                 ADMIN 99
WRITE(ISOUT,1) L,N                         ADMIN100
WRITE(ISOUT,2)                           ADMIN101
WRITE(ISOUT,3)                           ADMIN102
WRITE(ISOUT,4)                           ADMIN103
915  DO 920 K=1,KBHX                      ADMIN104
      UKNL=USUM(K,N,L)
      VKNL=VSUM(K,N,L)
      IF(ABS(UKNL)-1.0E-30) 9151,9154,9154  ADMIN105
9151 IF(ABS(VKNL)-1.0E-30) 9152,9153,9153  ADMIN106
9152 RKNL=0.                               ADMIN107
      GO TO 9155                           ADMIN108
9153 RKNL=1.57079633                      ADMIN109
      GO TO 9155                           ADMIN110
                                            ADMIN111
                                            ADMIN112
                                            ADMIN113
                                            ADMIN114
                                            ADMIN115
                                            ADMIN116

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9154	RKNL=ATAN(VKNL/UKNL)	ADMIN117
9155	DXKNL=DXSUM(K,N,L)	ADMIN118
	DYKNL=DYSUM(K,N,L)	ADMIN119
	IF(K-KBHX) 916,9156,920	ADMIN120
9156	RSUM(K,N,L)=RKNL	ADMIN121
	GO TO 9195	ADMIN122
916	ZSTEP=ZBH(K+1)-ZBH(K)	ADMIN123
	USUM(K,N,L)=UKNL*ZSTEP	ADMIN124
	VSUM(K,N,L)=VKNL*ZSTEP	ADMIN125
	RSUM(K,N,L)=RKNL*ZSTEP	ADMIN126
	DXSUM(K,N,L)=DXKNL*ZSTEP	ADMIN127
	DYSUM(K,N,L)=DYKNL*ZSTEP	ADMIN128
	DSUM=ZSTEP*DFZ(K,N,L)	ADMIN129
	M=K-1	ADMIN130
	IF(M) 920,919,918	ADMIN131
918	USUM(K,N,L)=USUM(K,N,L)+USUM(M,N,L)	ADMIN132
	VSUM(K,N,L)=VSUM(K,N,L)+VSUM(M,N,L)	ADMIN133
	RSUM(K,N,L)=RSUM(K,N,L)+RSUM(M,N,L)	ADMIN134
	DXSUM(K,N,L)=DXSUM(K,N,L)+DXSUM(M,N,L)	ADMIN135
	DYSUM(K,N,L)=DYSUM(K,N,L)+DYSUM(M,N,L)	ADMIN136
919	DKAV=DKAV+DSUM	ADMIN137
9195	IF(MC(1).LT.1) GO TC 920	ADMIN138
	WRITE(ISOUT,5) K,UKNL,VKNL,WFZ(K,N,L),DXKNL,DYKNL,DFZ(K,N,L),RKNL	ADMIN139
920	CONTINUE	ADMIN140
	IF(MC(1).NE.2) GO TC 9205	ADMIN141
	WRITE(ISOUT,6)	ADMIN142
	WRITE(ISOUT,7) (K,USUM(K,N,L),VSUM(K,N,L),DXSUM(K,N,L),	ADMIN143
	2DYSUM(K,N,L),RSUM(K,N,L),K=1,KBHX)	ADMIN144
9205	DKAV=DKAV/ZSPAN	ADMIN145
	WRITE(ISOUT,8) L,N, DKAV	ADMIN146
	CALL CNTR(NET,NETSU,N,XG,YG,ICF,JCF,NCF)	ADMIN147
	XQ=XG	ADMIN148
	YQ=YG	ADMIN149
	CALL NEST(NET,NETSU,XQ,YQ,NDATO,XL,XR,YL,YU,ICF,JCF,NCF)	ADMIN150
	AREAN=(XR-XL)*(YU-YL)	ADMIN151
	DAVG(L)=DAVG(L)+DKAV*AREAN	ADMIN152
	DO 9210 KL=1,KBHX	ADMIN153
9210	WAVG(KL,L)= WAVG(KL,L) + WFZ(KL,N,L)*AREAN	ADMIN154
921	CONTINUE	ADMIN155
	DAVG(L)=DAVG(L)/AREA	ADMIN156
	DO 9215 KL=1,KBHX	ADMIN157
9215	WAVG(KL,L)=WAVG(KL,L) / AREA	ADMIN158
	WRITE(ISOUT,15) L, DAVG(L)	ADMIN159
	WRITE(ISOUT,16)	ADMIN160
	WRITE(ISOUT,17) (K,WAVG(K,L),K=1,KBHX)	ADMIN161
922	CONTINUE	ADMIN162
	RETURN	ADMIN163
	END	ADMIN164

C SUBROUTINE ADVEC(NET,NETSU,ZBH,TIMUP,USUM,VSUM,DXSUM,DYSUM,RSUM,  
 C 1TDEP,CAV,PMAS,PSIZ,ICF,JCF,NCF,KBHF,NDATF,LTIMF,CAVS,WFZ)  
 C SEPTEMBER, 1971  
 C SUBROUTINE ADVEC TRANSPORTS PARCELS BY SIMPLE ADVECTION PLUS  
 C SETTLING. PARCEL TOP AND BASE ARE TRANSPORTED SEPARATELY, AND THE  
 C RESULTS ARE Smeared. THE COMMON VARIABLE ZP IS REDEFINED HEREIN.  
 C ZP - PARCEL CENTER Z COORDINATE BEFORE ADVECTION, EXCEPT AS  
 C REDEFINED IN SUB. ADVEC  
 COMMON /QPARM/ IPOINT,IPARIN,NBLK ,NAT ,NDELT ,KX ,KKM  
 1,NSEQO ,ICX ,JCX ,NCX ,KBHX ,NDATX ,LTIMX ,ISIN ,ISOUT  
 2,EDDY ,FMBEL ,LSTEP ,MC(18),WINT ,XLLC ,YLLC ,THETA ,ZHIN  
 3,CSKIP ,MINT ,ZMAX ,TIMEX ,DT ,DZ ,XP ,YP ,ZP  
 4,DINCR ,DOWN ,TP ,ZLOW ,DHAF ,RWAF ,ROPART,ZUPP ,VETA  
 5,DOPEN ,CROSS ,TIME ,KKMA1 ,KKX ,KKXS1 ,KXMIN ,NDATP  
 DIMENSION NET(ICF,JCF),NETSU(NCF),ZBH(KBHF),USUM(KBHF,NDATF,LTIMF)  
 DIMENSION VSUM(KBHF,NDATF,LTIMF),DXSUM(KBHF,NDATF,LTIMF)  
 DIMENSION DYSUM(KBHF,NDATF,LTIMF),TIMUP(LTIMF)  
 DIMENSION RSUM(KBHF,NDATF,LTIMF)  
 DIMENSION CAVS(KBHF),WFZ(KBHF,NDATF,LTIMF)  
 MC3=MC(3)  
 EPS=0.1  
 NDEP=0  
 ZDEP=ZMIN  
 CHANGE ZP FROM PARCEL CENTER TO PARCEL BASE ALTITUDE.  
 ZP=ZLOW  
 CALCULATE TRANSPORT OF PARCEL BASE.  
 IF ( (ZP-ZDEP).LE.EPS) GO TO 1411  
 CALL TRANP(NET,NETSU,ZBH,TIMUP,USUM,VSUM,DXSUM,DYSUM,RSUM,  
 1NDEP,TDEP,ZDEP,XOL,YOL,ZOL,TOL,SIGXL,SIGYL,ROL,NDATL,ICF,JCF,NCF,  
 2KBHF,NDATF,LTIMF,0,CAVS,WFZ)  
 GO TO 1412  
 1411 TOL=TP  
 XOL=XP  
 YOL=YP  
 ZOL=ZP  
 ROL=0.  
 SIGXL=RWAF  
 SIGYL=RWAF  
 CHANGE ZP FROM PARCEL BASE TO PARCEL TOP ALTITUDE.  
 1412 ZP=ZLOW+DHAF  
 CALCULATE TRANSPORT OF PARCEL TOP.  
 IF( ZP-ZDEP .LE.EPS) GO TO 1414  
 CALL TRANP(NET,NETSU,ZBH,TIMUP,USUM,VSUM,DXSUM,DYSUM,RSUM,  
 1NDEP,TDEP,ZDEP,XOU,YOU,ZOU,TOU,SIGXU,SIGYU,ROU,NDATU,ICF,JCF,NCF,  
 2KBHF,NDATF,LTIMF,0,CAVS,WFZ)  
 GO TO 1415  
 1414 TOU=TP  
 XOU=XP  
 YOU=YP  
 ZOU=ZP  
 ROU=0.  
 SIGXU=RWAF  
 SIGYU=RWAF  
 CALCULATE SHEAR OF PARCEL TOP AND BASE RESULTS.  
 1415 ZOUTN=(ZOL+ZOU)/2.  
 TOUTW=(TOL+TOU)/2.  
 IF(Abs(XOU-XOL).GE.1.0E-30) GO TO 1404  
 IF(Abs(YOU-YOL).GE.1.0E-30) GO TO 1403

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ROUTN=0.                                ADVEC 59
GO TO 1405                               ADVEC 60
1403 ROUTN=1.57079533                   ADVEC 61
GO TO 1405                               ADVEC 62
1404 ROUTN=ATAN((YOU-YOL)/(XOU-XOL))   ADVEC 63
1405 R=ROUTN-ROU                         ADVEC 64
SXL=1./SQRT((COS(R)/SIGXL)**2+(SIN(R)/SIGYL)**2)  ADVEC 65
SYL=1./SQRT((SIN(R)/SIGXL)**2+(COS(R)/SIGYL)**2)  ADVEC 66
R=ROUTN-ROU                         ADVEC 67
SXU=1./SQRT((COS(R)/SIGXU)**2+(SIN(R)/SIGYU)**2)  ADVEC 68
SYU=1./SQRT((SIN(R)/SIGXU)**2+(COS(R)/SIGYU)**2)  ADVEC 69
SXOTN=(SXU+SXL+SQRT((XOU-XOL)**2+(YOU-YOL)**2))/2.  ADVEC 70
SYOTN=SORT(SYU*SYL)                     ADVEC 71
XOUTN=XOL+(SXOTN-SXL)*COS(ROUTN)        ADVEC 72
YOUTN=YOL+(SXOTN-SXL)*SIN(ROUTN)        ADVEC 73
CALL SUMPER(XOUTH,YOUTH,ZOUTH,TOUTN,SXOTN,SYOTN,PHAS,PSIZ,ROUTN,1,ADVEC 74
11SDUT,IPOUT,MC3,NBLK)
RETURN                                 ADVEC 75
END                                    ADVEC 76
                                         ADVEC 77

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SUBROUTINE AMBN(TCH,DFZ,WFZ,ZHT,H,DIFF,AA,BB,CC,DENOM,E,F,NET, AMPNT 1
1NETSU,ZRH,TIMUP,USUM,VSUM,DXSUM,DYSUM,RSUM,NTRIP,LTIM,ICF,JCF,NCF,AMPNT 2
2KBHF,NDATF,LTIMF,KKF,CAVS) AMPNT 3
SEPTEMBER 1971 AMPNT 4
SUBROUTINE AMBN DETERMINES FROM INPUT FALL RATE AND VERTICAL WIND AMPNT 5
AND TURBULENCE DATA THE COEFFICIENT DATA VECTORS AMPNT 6
AA(K)=S2*(DIFF(K+1)+DIFF(K))+S1*F(K+1), AMPNT 7
BB(K)=S2*(DIFF(K+1)+2.*DIFF(K)+DIFF(K-1))+S1*F(K), AMPNT 8
CC(K)=S2*(DIFF(K)+DIFF(K-1)), AMPNT 9
DENOM(K)=1+THETA*(BB(K)-CC(K))*E(K-1), AMPNT 10
E(K)=THETA*AA(K)/DENOM(K), AMPNT 11
WHERE AMPNT 12
S1=DT/DZ, AMPNT 13
S2=DT/(2.* (DZ)**2)), AMPNT 14
AND F IS A TEMPORARY WORKING SPACE FOR VERTICAL VELOCITIES. AMPNT 15
NOTE THAT Q(K) FOR THE NEXT TIME STEP IS GIVEN BY AMPNT 16
AA(K)*Q(K+1)-BB(K)*C(K)+CC(K)*Q(K-1). AMPNT 17
DFXS1- VERTICAL DIFFUSIVITY AT ALTITUDE INCREMENT KX-1 AMPNT 18
LTIM - ATMOS. UPDATE INDEX FOR ARRAYS DFZ AND WFZ AMPNT 19
NTRIP - OPTION CODE FOR HORIZONTAL ADVECTION OF MASS ALOFT AMPNT 20
POSITIVE IF NDATO IS STORED IN NTRIP AMPNT 21
NEGATIVE IF NDATO IS TO BE FOUND VIA CALL TO SUB. TRNP AMPNT 22
COMMON /OPARM/ IPOUT,IPARIN,NBLK ,NAT ,NDELT ,KX ,KKM AMPNT 23
1,NSEOO ,ICX ,JCX ,NCX ,KRHX ,NDATX ,LTIMX ,ISIN ,ISOUT AMPNT 24
2,EDDY ,FMBEL ,LSTEP ,MC(15),WINT ,XLLO ,YLLC ,THETA ,ZMIN AMPNT 25
3,CSKIP ,MINT ,ZMAX ,TIMEX ,DT ,GZ ,XP ,YP ,ZP AMPNT 26
4,DINCR ,DOWN ,TP ,ZLOW ,DWAF ,PKAF ,ROPART ,ZUPP ,VETA AMPNT 27
5,DOPEN ,CROSS ,TIME ,KKMA1 ,KKX ,KKXS1 ,KXMIN ,NDATP AMPNT 28
COMMON /ODR/DFXS1,EFLUX,FMAB,PHI,THETO AMPNT 29
DOUBLE PRECISION AA(KKF),BB(KKF),CC(KKF),DENOM(KKF),E(KKF),F(KKF) AMPNT 30
DIMENSION DIFF(KKF),H(KKF),ZHT(KKF),DFZ(KBH),NDATF,LTIMF) AMPNT 31
DIMENSION WFZ(KBH),NDATF,LTIMF),TIMUP(LTIMF),ZBH(KBH),ZCH(KBH) AMPNT 32
DIMENSION OXSUM(KBH),NDATF,LTIMF)*DYSUM(KBH),NDATF,LTIMF) AMPNT 33
DIMENSION USUM(KBH),NDATF,LTIMF),VSUM(KBH),NDATF,LTIMF) AMPNT 34
DIMENSION RSUM(KBH),NDATF,LTIMF),NET(ICF,JCF),NETSU(NCF) AMPNT 35
DIMENSION CAVS(KBH)
DOUBLE PRECISION DFKXS1,EFLUX,FMAB,PHI,THETO AMPNT 36
DOUBLE PRECISION S1,S2 AMPNT 37
DATA PROGRM/#AMBN/#
CONSTRUCT F AND DIFF FOR K=0,=..,KX AMPNT 38
NDEP=100 AMPNT 39
TDEP=TIME AMPNT 40
NDATO=IABS(NTRIP)
COMPUTE KBH AND INITIALIZE AMPNT 41
DIFF(KKH)=0. AMPNT 42
F(KKH)=0. AMPNT 43
ZOLD=ZHT(KKH)
DOLD=DIFF(KKH)
FOLD=F(KKH)
DO 1 K=1,KBH
KBH=K
ZNEW=ZCH(<BH)
IF(ZOLD.LT.ZNEW) GO TO 2
1 IF(KBH.EQ.KBH) CALL ERROR(PROGRM,-1,ISOUT)
2 IF(NTRIP.LT.-1)
1CALL TRNP(NET,NETSU,ZBH,TIMUP,USUM,VSUM,DXSUM,DYSUM,RSUM, AMPNT 56
2NDEP,TDEP,ZNEW,YO,YC,ZC,TO,SIGYO,SIGZO,RO,NDATO,ICF,JCF,NCF,KBH, AMPNT 57
3NDATF,LTIMF,1,CAVS,WFZ) AMPNT 58

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DNEW=DFZ(KRH,NDATO,LTIM)
FNEW=-WFZ(KRH,NDATO,LTIM)
DSLOPE=(DNEW-DOLD)/(ZNEW-ZOLD)
FSLOPE=(FNEW-FOLD)/(ZNEW-ZOLD)
DO 5 KK=KKM1,KKX
ZHTKK=ZHT(KK)
IF(ZHTKK.LT.ZNEW) GO TO 4
JF(KBH.LT.KBHX-1) GO TO 3
40 DIFF(KK)=DNEW
F(KK)=FNEW
GO TO 5
3 KBH=KBH+1
IF(ZHTKK.GE.ZCH(KBH)) GO TO 30
DOLD=DNEW
FOLD=FNEW
ZOLD=ZNEW
GO TO 38
30 KBC=KRH+1
IF(KBC.LT.KBHX-1) GO TO 32
KBH=KBC
31 ZNEW=ZCH(KBH)
IF(INTRIP.LT.-1)
1CALL TRANP(NET,NFTSU,ZBH,TIMUP,USUM,VSUM,DXSUM,DYSUM,RSUM,
2NDEP,TDEP,ZNEW,X0,YC,Z0,TO,SIGX0,SIGY0,P0,NDATO,ICF,JCF,NCF,KPHF,
3NDATF,LTIMF,1,CAVS,WFZ)
DNEW=DFZ(KBH,NDATO,LTIM)
FNFW=-WFZ(KRH,NDATO,LTIM)
GO TO 46
32 KBHXM1=KBHX-1
DO 35 K=KBC,KBHXM1
KRH=K
IF(ZHTKK.GE.ZCH(KRH)) GO TO 35
ZOLD=ZCH(KRH-1)
IF(INTRIP.LT.-1)
1CALL TRANP(NET,NETSU,ZBH,TIMUP,USUM,VSUM,UXSUM,DYSUM,PSUM,
2NDEP,TDEP,ZOLD,X0,YC,Z0,TO,SIGX0,SIGY0,P0,NDATO,ICF,JCF,NCF,KRF,
3NDATF,LTIMF,1,CAVS,WFZ)
DOLG=DFZ(KRH-1,NDATO,LTIM)
FOLD=WFZ(KRH-1,NDATO,LTIM)
GO TO 38
35 CONTINUE
GO TO 31
38 ZNEW=ZCH(KBH)
IF(INTRIP.LT.-1)
1CALL TRANP(NET,NFTSU,ZBH,TIMUP,USUM,VSUM,DXSUM,DYSUM,RSUM,
2NDEP,TDEP,ZNEW,X0,YC,Z0,TO,SIGX0,SIGY0,P0,NDATO,ICF,JCF,NCF,KHF,
3NDATF,LTIMF,1,CAVS,WFZ)
DNEW=DFZ(KBH,NDATO,LTIM)
FNEW=-WFZ(KBH,NDATO,LTIM)
DSLOPE=(DNEW-DOLD)/(ZNEW-ZOLD)
FSLOPE=(FNEW-FOLD)/(ZNEW-ZOLD)
4 DIFF(KK)=DOLG+DSLOPE*(ZHTKK-ZOLD)
F(KK)=FOLD+FSLOPE*(ZHTKK-ZOLD)
5 CONTINUE
CORRECT DIFFUSIVITIES FOR CROSSING TRAJECTORIES EFFECTS
DO 150 KK=KKM,KKX
150 DIFF(KK)=DOWN*DIFF(KK)
COMBINE STILL-AIR FALL RATES WITH VERTICAL WINDS

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DO 250 KK=KKM,KXX          AMBNT117
250 F(KK)=F(KK)+H(KK)      AMPNT118
COMPUTE E(0) IN ACCORDANCE WITH REFLECTIVITY CONTROL VARIABLE VETA   AMPNT119
E(KKM)=U.                  AMPNT120
IF(VETA.LT.0.) GO TO 17     AMPNT121
WREF=F(KKH21)               AMPNT122
DRFF=(DIFF(KKH1)+DIFF(KKMA1))/(2.*DZ)    AMPNT123
E(KKM)=(WREF+DRFF)/(VETA+DREF)  AMPNT124
COMPUTE AA,BB,CC,DENOM, AND E FOR K=1,...,KX-1  AMPNT125
17 S2=DZ                   AMPNT126
S1=DT                      AMPNT127
S1=S1/S2                   AMPNT128
S2=S1/(2.*S2)              AMPNT129
DO 18 KK=KKMA1,KXX          AMPNT130
18 CC(KK)=S2*(DIFF(KK)+DIFF(KK-1))  AMPNT131
DO 19 KK=KKM,KKXS1           AMPNT132
19 AA(KK)=CC(KK+1)+S1*F(KK+1)  AMPNT133
DO 20 KK=KKM1,KKXS1          AMPNT134
BB(KK)=AA(KK-1)+CC(KK+1)    AMPNT135
DENOM(KK)=1.+THETQ*(BB(KK)-CC(KK)*E(KK-1))  AMPNT136
20 E(KK)=THETQ*AA(KK)/DENOM(KK)  AMPNT137
DFKKS1=DIFF(KKXS1)          AMPNT138
C WRITE(ISOUT,2221)          AMPNT139
C2221 FORMAT(*0CONTENTS OF ARRAYS ZHT, F, DIFF, AA, BB, CC, DENOM, E*)  AMPNT140
C KRITE(ISOUT,2222) ZHT      AMPNT141
C KRITE(ISOUT,2222) F        AMPNT142
C KRITE(ISOUT,2222) DIFF    AMPNT143
C KRITE(ISOUT,2222) AA       AMPNT144
C KRITE(ISOUT,2222) BB       AMPNT145
C KRITE(ISOUT,2222) CC       AMPNT146
C KRITE(ISOUT,2222) DENOM   AMPNT147
C KRITE(ISOUT,2222) E        AMPNT148
C2222 FORMAT(*0*(13E10.2))  AMPNT149
RETURN                      AMPNT150
END                         AMPNT151

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SUBROUTINE SPRVS(NET,NETSU,ZBH,ZCH,TIMUP,USUM,VSUM,OXSUM,DYSUM,
1RSUM,DFZ,WFZ,DAVG,WAVG,ALT,RHO,ATEMP,AA,BB,CC,DENOM,DIFF,E,F,Q,W,
2ZHT,ICF,JCF,NCF,KBHF,NCATF,LTIMF,KKF,NATF,CAVS)
C SEPTEMBER 1971
C SUBROUTINE SPRVS SUPERVISES DIFFUSIVE AND/OR ADVECTIVE TRANSPORT
C OF FALLOUT PARCELS LISTED ON TAPE IPARIN. PARCEL PARAMETERS ARE
C STORED IN ARRAYS XPAR, YPAR, ZPAR, TPAM, PSAM, RWFR, DWFR, ZLWF, VWFR
C ONLY ONE PARCEL IS TRANSPORTED AT A TIME. FOR THIS PARCEL ABOVE
C ITEMS ARE STORED IN XP,YP,ZP,TP,PSIZ,PMAS,RWAF,DWAF,ZLOW,VHAF.
C XPAR - X COORDINATE OF PARCEL CENTER DATA VECTOR (AT TIME TPAR)
C YPAR - Y COORDINATE OF PARCEL CENTER DATA VECTOR (AT TIME TPAR)
C ZPAR - Z COORDINATE OF PARCEL CENTER DATA VECTOR (AT TIME TPAR)
C TPAR - TIME OF DEFINITION OF CLOUD PARCEL DATA VECTOR
C PMAM - MIDPOINT OF PARCEL PARTICLE SIZE CLASS DATA VECTOR
C PSA'4 - TOTAL MASS OF PARCEL DATA VECTOR (AT TIME TPAR)
C RWFR - RADIUS OF PARCEL AT C. O. M. DATA VECTOR (AT TIME TPAR)
C DWFR - PARCEL THICKNESS DATA VECTOR (AT TIME TPAR)
C ZLWF - ALTITUDE OF PARCEL BASEA DATA VECTOR (AT TIME TPAR)
C VWFR - PARCEL VOLUME DATA VECTOR (AT TIME TPAR)
COMMON /QPARM/ IPOINT,IPARIN,NBLK ,NAT ,NDELT ,KX ,KKM
1,NSEQO ,ICX ,JCX ,NCX ,KBHX ,NDATX ,LTIMX ,ISIN ,ISOUT
2,EODY ,FMBEL ,LSTEF ,MC(13),WINT ,XLLC ,YLLC ,THETA ,ZMIN
3,CSKIP ,MINT ,ZMAX ,TIMEX ,DT ,DZ ,XP ,YP ,ZP
4,DINCR ,DOWN ,TP ,ZLOW ,DWAF ,RWAF ,ROPART,ZUPP ,VFTA
5,DOPEN ,CROSS ,TIE ,KKMA1 ,KX ,KKXS1 ,KXMIN ,NDATP
COMMON /QDBLE/DFKXS1,EFFFLUX,FMAB,PHI,THETG
DOUBLE PRECISION AA(KKF),BB(KKF),CC(KKF),DENOM(KKF),E(KKF),F(KKF)
DOUBLE PRECISION Q(KKF)
DIMENSION ALT(NATF),RHO(NATF),ATEMP(NATF)
DIMENSION NET(ICF,JCF),NETSU(NCF),ZBH(KBHF),ZCH(KBHF),DIFF(KKF)
DIMENSION USUM(KBHF,NDATF,LTIMF),VSUM(KBHF,NDATF,LTIMF),W(KKF)
DIMENSION DXSUM(KBHF,NDATF,LTIMF),DYSUM(KBHF,NDATF,LTIMF)
DIMENSION DFZ(KBHF,NDATF,LTIMF),ZHT(KKF)
DIMENSION WFZ(KBHF,NDATF,LTIMF),DAVG(LTIMF),WAVG(KBHF,LTIMF)
DIMENSION TIMUP(LTIMF),RSUM(KBHF,NDATF,LTIMF)
DIMENSION XPAR(100),YPAR(100),ZPAR(100),TPAM(100)
DIMENSION PSAM(100),RWFR(100),DWFR(100),ZLWF(100),VWFR(100)
DIMENSION CAVS(KBHF)
DOUBLE PRECISION DFKXS1,EFFFLUX,FMAB,PHI,THETQ
8014 FORMAT(#+#T102,E12.4,I4)
8015 FORMAT(#+#T103, #AIREORNE (ADVCN) #)
8016 FORMAT(#+#I4,9E12.4)
8017 FORMAT(#+#T103, #AIREORNE (DIFFN) #)
8018 FORMAT(#+#T103, #ADVECTIVE TRNSPT#)
8019 FORMAT(#+#T103, # IMPACTED WAFER#)
8020 FORMAT(#+#T103, #OUTSIDE WINDGRID#)
8021 FORMAT(#+#36X, #PARTICLE SIZE CLASS#E12.4, # MICRONS#)
8022 FORMAT(#+#22X, #FALL RATE#E12.4, # METERS/SEC AT ALTITUDE#E12.4, #
1 METERS/#22X, #UPPER LIMIT INPUT ALTITUDE FOR ADV. TRANSP. IS#E12.4#
2, # METERS#)
8024 FORMAT(#+#T2, #NSEQ#11, #XP#T23, #YP#T35, #ZP#T47, #TP#T58, #PMAS#T70, #SPRVS 51
1RWAF#T92, #ZLOW#T94, #DWAF#T107, #DZ#T115, #KX#/)
8025 FORMAT(#ONEGATIVE DEPOSIT. WAFER NO.#I4, # AT TIME#E12.4, #. VARIABLSPRVS 53
SES EFFFLUX,FMAB,DEP #2D12.4,E12.4#)
DATA PROGRM/#SPRVS #/
JF=100
KKMA1=1,KM+1
THETO=THETA

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PHI=1.-THETO          SPRV5 59
KXBF=0               SPRV5 60
MC3=MC(3)            SPRV5 61
NSEQ=0               SPRV5 62
PSZBE=-2.0            SPRV5 63
COMPUTE OVERALL AVERAGE VERTICAL VELOCITY FOR THE FIRST UPDATE   SPRV5 64
WAVGK=0.0              SPRV5 65
KBHM1=KBHX-1           SPRV5 66
DO 50 K=1,KBHM1        SPRV5 67
 50 WAVGK=WAVGK + WAVG(K,1)*(ZBH(K+1) - ZBH(K))    SPRV5 68
  WAVGK=WAVGK/(ZBH(K+1)-ZBH(1))                     SPRV5 69
COMPUTE TIMEX MARGIN FACTOR FOR ADVECTIVE TRANSPORT AIRBORNE TEST   SPRV5 70
IF(NDATX-1)70,70,60      SPRV5 71
 60 SLOP=1.1             SPRV5 72
  GO TO 90               SPRV5 73
 70 SLOP=1.0             SPRV5 74
COMPUTE MINIMUM SMALL ALTITUDE INCREMENT DZMIN                   SPRV5 75
 80 DZMIN=(ZMAX-ZMIN)/KX                                     SPRV5 76
CUE IPARIN TAPE AT BEGINNING OF INPUT PARCEL BLOCK             SPRV5 77
100 READ(IPARIN) NP                                         SPRV5 78
  IF(NP.LE.0) GO TO 805                                     SPRV5 79
  IF(NP.GT.JF) CALL ERROR(PROGRM,-100,ISOUT)                SPRV5 80
COPY IN A BLOCK OF INPUT PARCEL PARAMETERS FROM TAPE IPARIN       SPRV5 81
  READ(IPARIN) (XPAR(J),YPAR(J),ZPAR(J),TPAR(J),PDAM(J),PSAM(J),   SPRV5 82
  1RWFR(J),DWFR(J),ZLHF(J),VHFR(J),J=1,NP)                  SPRV5 83
COMMENCE PROCESSING BLOCK OF INPUT PARCELS ONE AT A TIME         SPRV5 84
  DO 1000 J=1,NP                                         SPRV5 85
  NSEQ=NSEQ+1                                         SPRV5 86
  IF(NSEQ.LT.NSEQ0) GO TO 1000                         SPRV5 87
  XP=XPAR(J)                                         SPRV5 88
  YP=YPAR(J)                                         SPRV5 89
  ZP=ZPAR(J)                                         SPRV5 90
  TP=TPAR(J)                                         SPRV5 91
  PSIZ=1.0E6*PDAM(J)                                SPRV5 92
  PMAS=PSAM(J)                                       SPRV5 93
  RWAF=RWFR(J)/2.                                     SPRV5 94
  DWAF=DWFR(J)                                       SPRV5 95
  ZLOW=ZLWF(J)                                       SPRV5 96
  VHAF=VHFR(J)                                       SPRV5 97
CHECK FOR NEW PARTICLE SIZE CLASS                           SPRV5 98
  IF(ABS((PSIZ-PSZBE)/PSIZ).LE.1.0E-10) GO TO 103        SPRV5 99
  WRITE(ISOUT,8021) PSIZ                                 SPRV5 100
COMPUTE MID-ATMOSPHERE FALL RATE FAV FOR NEW PARTICLE SIZE CLASS   SPRV5 101
  H=(ZMIN+ZMAX)/2.                                     SPRV5 102
  CALL TRPL(H,NAT,ALT,RHO,DEN)                        SPRV5 103
  CALL TRPL(H,NAT,ALT,ATEMP,VIS)                      SPRV5 104
  CALL FALRT(PSIZ,ROPART,H,DEN,VIS,FAV,ISOUT)        SPRV5 105
  FAV=FAV-WAVGK                                      SPRV5 106
COMPUTE UPPER LIMIT ALTITUDE FOR ADVECTIVE TRANSPORT OF THIS SIZE PART.   SPRV5 107
  CALL CALIB(ZBH,KBHX,ZMIN,-1,KBHZ)                    SPRV5 108
  CALL TRPL(ZBH(KBHZ),NAT,ALT,ATEMP,VIS)              SPRV5 109
  CALL TRPL(ZBH(KBHZ),NAT,ALT,RHO,DEN)                SPRV5 110
  CALL FALRT(PSIZ,ROPART,ZBH(KBHZ),DEN,VIS,CAV,ISOUT)  SPRV5 111
  TDEP=TP + (ZBH(KBHZ) - ZMIN) /(CAV - WAVG(KBHZ-1,1))  SPRV5 112
  KBHM1=KBHX-1                                         SPRV5 113
  DO 1001 IZ=KBHZ,KRHM1                               SPRV5 114
  CALL TRPL(ZCH( IZ ),NAT,ALT,ATEMP,VIS)              SPRV5 115
  CALL TRPL(ZCH( IZ ),NAT,ALT,RHO,DEN)                SPRV5 116

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CALL FALRT(PSIZ, ROPART, ZCH( IZ ), DEN, VIS, CAV, ISOUT)           SPRVS117
TDEP=TDEP + (ZBH(IZ+1) - ZBH(IZ))/(CAV- WAVG(IZ,1))               SPRVS118
IF(TDEP.GT.SLOP*TIMEX) GO TO 1002                                     SPRVS119
1001 CONTINUF
ZLIM=5.0E4
GO TO 1003
1002 ZLIM=ZBH(IZ+1)
1003 WRITE(ISOUT,8022) FAV,H,ZLIM
WRITE(ISOUT,8024)
COMPUTE PARTICLE FALL RATE TABLE FOR EACH ATMOSPHERIC STRATUM WHEN
C A NEW PARTICLE SIZE IS ENCOUNTERED
DO 101 KKZ=1,KBHX
CALL TRPL(ZCH(KKZ),NAT,ALT,ATEMP,VIS)
CALL TRPL(ZCH(KKZ),NAT,ALT,RHO,DEN)
101 CALL FALRT(PSIZ, ROPART, ZCH(KKZ), DEN, VIS, CAVS(KKZ), ISOUT)   SPRVS126
COMPUTE DIFFUSIVITY CORRECTIONS FOR NEW PARTICLE SIZE CLASS
DOWN=(FAV*EDDY)**2
CROSS=1./SQRT(1.+4.*DOWN)
DOWN=1./SQRT(1.+DOWN)
PSZBE=PSIZ
103 WRITE(ISOUT,8016) NSEQ,XP,YP,ZP,TP,PMAS,RWAF,ZLOW,DWAF
CANCEL PROCESSING OF PARCEL IF IT HAS ALREADY IMPACTED
IF(IFIX(DWAF).GT.0) GO TO 1200
WRITE(ISOUT,8019)
CALL DUMPER(XP,YP,ZP,TP, RWAF, RWAF, PMAS, PSIZ,0.,0.,
1ISOUT,IPOUT,MC3,NALK)
GO TO 1000
COMPUTE INDFX OF MESH OR SUB-MESH CONTAINING PARCEL CENTER POSITION
1200 CALL NEST(NET,NETSU,XP,YP,NDATP,XL,XR,YL,YU,ICF,JCF,NCF)
CANCEL PROCESSING OF PARCEL IF IT IS INPUT OUTSIDE ATMOS.
IF(NDATP.GT.0) GO TO 1248
WRITE(ISOUT,8020)
GO TO 1000
COMPUTE AVERAGE FALL RATE CAV
1248 ZUPP=ZLOW+DWAF
ZL0=ZLCW-ZMIN
ZUP=ZUPP-ZMIN
H=ZMIN+ZUP/2.
CALL TRPL(H,NAT,ALT,RHO,DEN)
CALL TRPL(H,NAT,ALT,ATEMP,VIS)
CALL FALRT(PSIZ, ROPART, H, DEN, VIS, CAV, ISOUT)                   SPRVS150
CANCEL PROCESSING OF PARCEL IF IT WILL REMAIN AIRBORNE BY DIFFUSION
DAV=DOWN*DAVG(1)
CAV=CAV-WAVGK
TFLY=TIMEX-TP
IF(TFLY.LE.0.) GO TO 1249
CALL ESTM(ZUP,CAV,DAV,TFLY,PUP)
CALL ESTM(ZL0,CAV,DAV,TFLY,PLO)
PDEST=1.0-(PUP-PLO)/(ZUP-ZL0)
IF(GSKIP.LE.PDEST) GO TO 1250
1249 WRITE(ISOUT,8017)
GO TO 1000
COMPUTE TRANSPORT BY ADVECTION IF TRUNCATION ERROR IS EXCEEDED
1250 IF(DZMIN.LE.0.2*DAV/FAV) GO TO 1500
CANCEL PROCESSING OF PARCEL IF IT WILL REMAIN AIRBORNE BY ADVECTION
IF(ZLOW.LT.ZLIM) GO TO 1409
WRITE(ISOUT,8015)
GO .0 1000

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1409 WRITE(ISOOUT,8018)
      CALL      ADVEC(NET,NETSU,ZBH,TIMUP,USUM,VSUM,DXSUM,DYSUM,RSUM,
      1TDEP,CAV,PMAS,PSIZ,ICF,JCF,NCF,KBFH,NDATF,LTIMF,CAVS,WFZ)
      GO TO 1000
COMPUTE SMALL ALTITUDE INCREMENT DZ
1500 DZMAX=0WAF
1501 IF(DZMAX.GE.DZMIN) GO TO 1502
      DZMAX=2.0*DZMAX
      GO TO 1501
1502 D7=0.2*DAV/FAV
      IF(DZ.GT.DZMAX) DZ=DZMAX
      KX=(ZMAX-ZMIN)/DZ+1.
      IF(KX.LT.KXMIN) KX=KXMIN
      D7=(ZMAX-ZMIN)/KX
      WRITE(ISOOUT,8014) DZ,KX
COMPUTE ALTITUDE INCREMENT AND FALL RATE DATA VECTORS
      IF(K'.EQ.KXP) GO TO 1305
      KXX=KKM+KX
      KKXS1=KXX-1
      DO 1304 KK=1,KXX
      ZHT(KK)=ZMIN+DZ*(KK-KKM)
      CALL TRPL(ZHT(KK),NAT,ALT,RHO,DEN)
      CALL TRPL(ZHT(KK),NAT,ALT,ATEMP,VIS)
1304 CALL FALRT(PSIZ,ROFAPT,ZHT(KK),DEN,VIS,W(KK),ISOOUT)
      KXBE=KX
COMPOSE INITIAL CONCENTRATION DATA VECTOR
1305 CALL CONC(ZHT,0,KKF)
CANCEL PROCESSING OF WAFER IF INITIAL AIRBORNE MASS IS INADEQUATE
      IF(FMA9.LT.1) GO TO 1000
      DEPB=0.
      NTRIP=NDATP
COMPUTE FIRST DEPOSIT INCREMENT TIME INTERVAL TDELT
      TDELT=TFLY/NDELT
      TLARG=TDELT
      TAE=4.*ZUP/(3.*CAV)
      IF(TAE.LT.TFLY) TDELT=TAE/NDELT
      TSMAL=MINT*DT
      IF(TDELT.LT.TSMAL) TDELT=TSMAL
COMMENCE DEPOSIF TIME LOOP
      TIME=TP
      TPAUS=TIME
      LTIM=-1
      NPASS=1
      XOBEP=XP
      YOPEP=YP
      1 LSTEP=TDELT/DT +1.
      TDELT=LSTEP*DT
135 TPAUS=TPAUS+TDELT
COMPUTE DATA SET TIME INDEX LTIM
      CALL CALI9(TIMUP,LTIMX,TIME,+1,LTIMA)
      IF(LTIM.NE.LTIMA) GO TO 3
      IF(IABS(NTRIP)-1) 31,32,31
      3 LTIM=LTIMA
COMPOSE CONCENTRATION COEFFICIENT DATA ARRAYS
31 CALL AMBNT(ZCH,DFZ,WFZ,ZHT,W,DIFF,AA,BB,CC,DENGH,E,F,NET,
      1NETSU,ZBH,TIMUP,USUM,VSUM,DXSUM,DYSUM,RSUM,NTRIP,LTIM,ICF,JCF,NCF,SPRVS230
      2KBHF,NDATF,LTIMF,KKF,CAVS)
      NTRIP=-NDATX

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COMPUTE NUMBER OF ITERATIONS LSTEP OF SOLUTION TO VERTICAL DIFFUSION      SPRVS23?
C   DIFFERENCE EQUATION FOR THIS DEPOSIT INCREMENT TIME INTERVAL      SPRVS234
  32 IF(LTIM.GE.LTIMX) GC TO 138                                         SPRVS235
    IF(TPAUS.LT.TIMUP(LTIM+1)) GO TO 140                               SPRVS236
    TPAUS=TIMUP(LTIM+1)
    TDELT=TPAUS-TIME
    LSTEP=TDELT/DT+1.
    TDELT=LSTEP*DT
  138 IF(TPAUS.LT.TIMEX) GO TO 140                                     SPRVS237
    TPAUS=TIME
    TDELT=TPAUS-TIME
    LSTEP=TDELT/DT+1.
    TDELT=LSTEP*DT
    IF(LSTEP.LE.0) GO TO 1000                                         SPRVS238
  140 IF(NPASS.NE.1) GO TO 4                                           SPRVS239
    NPASS=2
    TDELT_P=TDELT
COMPUTE DEPOSIT INCREMENT FRACTIONAL MASS DEP                         SPRVS240
  4 CALL DIFFF(Q,AA,BB,CC,DENOM,E,F,DEP,KKF)                           SPRVS241
CHECK DEPOSIT INCREMENT FRACTIONAL MASS DEP AGAINST DOPEN               SPRVS242
  IF(DEP.GE.-DOPEN*TDELT) GO TO 5                                     SPRVS243
  WRITE(ISOOUT,3025) NSE0,TIME,EFFFLUX,FMAB,DEP
  5 IF(DEP.GE.DOPEN*TDELT) GO TO 7                                     SPRVS244
CHECK CUMULATIVE AIRBORNE FRACTIONAL MASS FMAB AGAINST FMBEL            SPRVS245
  IF(SNGL(FMAB).GT.FMPEL) GO TO 135                                 SPRVS246
  GO TO 1000
COMPARE RATE OF CHANGE OF DEPOSITION RATE DDPD WITH DINCR AND ADJUST     SPRVS247
C   NEXT TDELT
  7 DDPD=(DEP/TDELT)-(DEPRE/TDELT_B)/TDELT                          SPRVS248
  IF(DDPD.LT.DINCR) GC TO 10                                         SPRVS249
  TDELT_B=TDELT
  TDELT=TDELT/2.
  IF(TDELT.LT.TSMALL) TDELT=TSMALL
  GO TO 13
  10 IF(DDPD.GT.DINCR) GC TO 13
    TDELT_B=TDELT
    TDELT=2.*TDELT
    IF(TDELT.GT.TLARG) TDELT=TLARG
COMPUTE DEPOSIT INCREMENT MASS PMDEP                                     SPRVS250
  13 PMDEP=PMAS*DEP
    DEPRE=DEP
    NDEP=0
    ZDEP=ZMIN
    TDEP=TIME
COMPUTE DEPOSIT INCREMENT POSITION (X0,Y0,Z0) AND HORIZONTAL DISPERSION   SPRVS251
C   PARAMETERS (SIGX0,SIGY0,RO) AT TIME=TO
    CALL TRANP(NET,NETSU,ZBH,TIMUP,USUM,VSUM,DXSUM,DYSUM,PSUM,
    1NDEP,TDEP,ZDEP,X0,YC,Z0,TO,SIGX0,SIGY0,RC,NDATO,ICF,JCF,NCF,KBF,
    2NDATF,LTIMF,1,CAVS,WF7)
CONTINUE ON TO NEXT WAFER IF THIS ONE LIES OUTSIDE WINDFIELD             SPRVS252
  IF(NDATO.LE.0) GO TO 1000
COLLECT FINAL RESULTS FOR THIS WAFER AND STORE IN BUFFER DATA VECTORS     SPRVS253
  XH=(X0+X0BE)/2.
  YH=(Y0+Y0BE)/2.
  CALL DUMPER(XH,YH,Z0,TO,SIGX0,SIGY0,PMDEP,PSIZ,RO,0,
  1ISOOUT,IPOUT,MG3,NBLK)                                              SPRVS254
  X0BE=X0
  Y0BE=Y0

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IF(TIME+DT.LT.TIMEX) GO TO 1	SPRVS291
1000 CONTINUE	SPPVS292
GO TO 100	SPPVS293
COPY OUT BUFFER DATA VECTCRS. WAFER PROCESSING HAS BEEN COMPLETED	SPRVS294
806 CALL DUMPER(0.,0.,0.,0., 0., 0., 0., 0.,0.,999,	SPRVS295
1ISOUT,IPOUT,MC3,NBLK)	SPRVS296
CALL DUMPER(0.,0.,0.,0., 0., 0., 0., 0.,0.,999,	SPPVS297
1ICOUT,IPOUT,MC3,NBLK)	SPPVS298
REWIND IPARIN	SPRVS299
END FILE IPOUT	SPPVS300
REWIND IPOUT	SPPVS3G1
RETURN	SPPVS302
END	SPPVS303

SUBROUTINE TRANP(NET,NETSU,ZBH,TINUP,USUM,VSUM,DXSUM,DYSUM,RSUM, TRANP 1  
 1NDEP,TDEP,ZOEP,X0,YC,ZC,TO,SIGX0,SIGY0,R0,NDATO,ICF,JCF,NCF,KBFH, TRANP 2  
 2NDATF,LTIMF,KRIP,CAVS,WFZ) TRANP 3  
 SEPTEMBER 1971 TRANP 4  
 SUBROUTINE TRANP DETERMINES (AT AN INPUT TERMINAL ALTITUDE PLANE) TRANP 5  
 THE WAFER HORIZONTAL CENTER POSITION AND DISPERSION PARAMETERS FORTRANP 6  
 AN INPUT TRANSPORT FLIGHT TIME TRANP 7  
 CAVS - PARTICLE FALL RATE TABULATED FOR EACH ALTITUDE STRATUM TRANP 8  
 DXSUM - TURBULENCE X COMPONENT (WEIGHTED SUM) 3-DIM. DATA ARRAY TRANP 9  
 DYSUM - TURBULENCE Y COMPONENT (WEIGHTED SUM) 3-DIM. DATA ARRAY TRANP 10  
 NET - HORIZONTAL SPACE CONTROL NET MESH 2-DIM. ARRAY TRANP 11  
 NETSU - HORIZONTAL SPACE CONTROL NET SUB-MESH DATA VECTOR TRANP 12  
 RSUM - WIND HEADING ORIENTATION ANGLE (WEIGHTED SUM) 3-DIM. ARRAY TRANP 13  
 USUM - WIND X COMPONENT (WEIGHTED SUM) 3-DIM. DATA ARRAY TRANP 14  
 VSUM - WIND Y COMPONENT (WEIGHTED SUM) 3-DIM. DATA ARRAY TRANP 15  
 ZBH - ATMOSPHERE STRATA BASE-ALTITUDE DATA VECTOR TRANP 16  
 MODE - COMPUTATION MODE SWITCH TRANP 17  
     0 RAPID COMPUTATION TRANP 18  
     1 LAYERWISE COMPUTATION TRANP 19  
 NDEP - OPTION CONTROL VARIABLE TRANP 20  
     ZERO IF SIGX0 AND SIGY0 ARE TO BE COMPUTED TRANP 21  
     NON-ZERO IF SIGX0 AND SIGY0 ARE NOT TO BE COMPUTED AND  
         IF NDATO IS TO BE POSITIVE ALWAYS TRANP 22  
         TRANP 23  
 TDEP - ADVECTIVE TRANSPORT TIME INTERVAL TRANP 24  
 KRIP - CONTROL VARIABLE TRANP 25  
     0 FOR ADVECTIVE TRANSPORT TRANP 26  
     1 FOR DIFFUSIVE TRANSPORT TRANP 27  
 WFZ - VERTICAL WIND FIELD TRANP 28  
 ZOEP - ADVECTIVE TRANSPORT TERMINAL ALTITUDE TRANP 29  
 TO - TIME AFTER PARCEL ADVECTION TRANP 30  
 X0 - PARCEL CENTER X COORDINATE AFTER ADVECTION TRANP 31  
 Y0 - PARCEL CENTER Y COORDINATE AFTER ADVECTION TRANP 32  
 Z0 - PARCEL CENTER Z COORDINATE AFTER ADVECTION TRANP 33  
 SIGX0 - PARCEL MASS HOR. STAND. DEV. DOWNWIND AFTER ADVECTION TRANP 34  
 SIGY0 - PARCEL MASS HOR. STAND. DEV. CROSSWIND AFTER ADVECTION TRANP 35  
 NDATO - HORIZONTAL INDEX OF LATTICE CELL CONTAINING POINT (XC,YC) TRANP 36  
 R0 - WIND HEADING ORIENTATION ANGLE AFTER ADVECTION TRANP 37  
 COMMON /OPARM/ IFOUT,IPARIN,NBLK ,NAT ,NDELT ,KX ,KYM TRANP 38  
 1,PSOC ,ICX ,JCY ,NCX ,KBHX ,NDATX ,LTIMX ,ISIN ,ISCUT TRANP 39  
 2,EODY ,FMDEL ,LSTEP ,MC(15),WINT ,XLLS ,YLLC ,THETA ,ZMIN TRANP 40  
 3,CSKIP ,MINT ,ZMAX ,TIMEX ,DT ,DZ ,XP ,YP ,ZP TRANP 41  
 4,BINCP ,DCWN ,TP ,ZLOW ,DKAF ,RWAF ,ROPART,ZUPP ,VETA TRANP 42  
 5,OPEN ,CROSS ,TIME ,KKHA1 ,KXX ,KKXS1 ,KXMIN ,NDATF TRANP 43  
 DIMENSION NET(ICF,JCF),NETSU(NCF),ZBH(KBFH),USUM(KBFH,NDATF,LTIMF) TRANP 44  
 DIMENSION VSUM(ZBH,NDATF,LTIMF),DXSUM(KBFH,NDATF,LTIMF)  
 DIMENSION DYSUM(KBFH,NDATF,LTIMF),TINUP(LTIMF)  
 DIMENSION CAVS(KBFH)  
 DIMENSION RSUM(KBFH,NDATF,LTIMF)  
 DIMENSION WFZ(KBFH,NDATF,LTIMF)  
 DATA PROGRM/\*TRANP \*/  
 2 FORMAT(\* TIME=ZE12.4,%. ALT=ZE12.4,%. X-POS=ZE12.4,%. Y-POS=ZE12.4) TRANP 51  
 2,%. CELL=IZ,%. REACHED%) TRANP 52  
 3 FORMAT(\* TIME=ZE12.4,%. ALT=ZE12.4,%. X-POS=ZE12.4,%. Y-POS=ZE12.4) TRANP 53  
 3,%. CELL=IZ,%. ATTEMPTED%) TRANP 54  
 4 FORMAT(\*WAFFER WITH INITIAL CONFIGURATION XP,YP,ZP,TP #4E12.4/#REQTRANP 55  
 REQUIRED CHANNELLING AT CONFIGURATION XC,YC,ZC,TC #4E12.4)  
 EPSILO=.0005 TRANP 56  
 EPS=EPSILO\*WINT TRANP 57  
 TRANP 58

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EPSI=EPSILO*TDEP          TRANP 59
EPSI=.1                   TRANP 60
X0=XP                   TRANP 61
Y0=YP                   TRANP 62
Z0=ZP                   TRANP 63
T0=TP                   TRANP 64
SIGX0=0.                 TRANP 65
SIGY0=0.                 TRANP 66
R0=0.                    TRANP 67
NDACTC=NDACTR            TRANP 68
NDTC1=0                  TRANP 69
NDTO1=0                  TRANP 70
KBHC1=0                  TRANP 71
KBHO1=0                  TRANP 72
1000 CONTINUE             TOANP 73
KAY=-1                  TRANP 74
IF (KRIP.EQ.1) GO TO 50   TRANP 75
CALCULATE FALL VELOCITY FOR ADVECTION ON BASIS OF LOCAL
C    FALL RATE AND WIND FIELD AND STORE IN WBAR           TRANP 76
C    CALL CALIB(ZBH,KBHX,Z0,KAY,KBH2)
CALL CALIB(TIMUP,LTIMX,T0,1,LTIM)                      TRANP 78
WBAR=WFZ(KBH2-1,NDACTO,LTIM)-CAYS(KBH2-1)            TRANP 79
IF (WBAR) 112,111,110                                     TRANP 80
COMPUTE THE VERTICAL PSEUDO-VELOCITY WBAR AND STORE ITS SIGN IN KAY
C    FOR THE DIFFUSIVE SFTTLNG CASE                         TRANP 81
50  WBAR=(ZDEP-ZP)/(TDEF-TP)                                TRANP 82
IF(WPAR) 112,111,110                                     TRANP 83
110 KAY=KAY+1                                              TRANP 84
111 KAY=KAY+1                                              TRANP 85
112 CONTINUE                                              TRANP 86
CALIBRATION OF ZDEP AGAINST ZRH YIELDS TERMINAL ZBH-PLANE
IF (KRIP.EQ.1) CALL CALIB(ZBH,KBHX,ZDEP,KAY,KBH)        TRANP 87
CONSIDER KAY=0 CASE INDEPENDENTLY                         TRANP 88
200 IF(KAY.NE.0) GO TO 206                                 TRANP 89
IF (KRIP.EQ.1) GO TO 205                                 TRANP 90
C    IN THE ADVECTIVE TRANSPORT CASE WHENEVER THE ACTUAL FALL RATE
C    IS ZERO THEN SET THE DEPOSITION TIME INCREMENT EQUAL TO THE
C    TIME LEFT BEFORE THE WIND FIELD IS UPDATED             TRANP 91
C    TSEG=TIMUP(LTIM+1)-T0                                  TRANP 92
KBHC=KBHZ+1                                              TRANP 93
KBHO=KBHZ                                              TRANP 94
GO TO 300                                                 TRANP 95
205 TSEG=TDEF-T0                                         TRANP 96
NONE=1                                                    TRANP 97
KBHC=KBH
KBHO=KBHC-1                                             TRANP 98
GO TO 300                                                 TRANP 99
CALIBRATION OF Z0 AGAINST ZBH YIELDS CURRENT ZBH-PLANE
206 CALL CALIB(ZBH,KBHX,Z0,-KAY,KTRY)                   TRANP 100
CALL CALIB(ZBH,KBHX,Z0,+KAY,KSHC)                      TRANP 101
IF (KRIP.EQ.0).OR.(KBHO.NE.KTRY) GO TO 213             TRANP 102
CONSIDER EXCURSION TO TERMINAL ZBH-PLANE
KBHC=KBH
ZEST=ZBH/KBHC                                           TRANP 103
NONE=0                                                    TRANP 104
IF(KAY*(KBHO-KBHC)+17 .GT. 211,213,218)               TRANP 105
CONSIDER EXCURSION BETWEEN ADJACENT ZBH-PLANES
213 KBHC=KBHC+KAY                                         TRANP 106

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ZEST=ZAH(KRHC)          TRANP117
MODE=1                   TRANP118
IF((KBHC.LE.<BHX).AND.(KAY*ZEST.LE.KAY*ZDEP)) GO TO 221  TRANP119
CONSIDER EXCURSION TO TERMINAL ZDEP-PLANE
210 KBHC=KRHO+KAY        TRANP120
ZEST=ZDEP                TRANP121
MODE=1                   TRANP122
TRANP123
221 TSEG=(ZEST-Z0)/WBAR   TRANP124
CHECK IF UPDATE TIME BOUNDARY WILL BE CROSSED
300 TC=T0+TSEG            TRANP125
CALL CALIB(TIMUP,LTIMX,T0,1,LTIM)           TRANP126
IF((LTIM.LT.LTIMX).AND.(TIMUP(LTIM+1).LE.TC)) TSEG=TIMUP(LTIM+1)-T0  TRANP127
COMPUTE AVERAGE HORIZONTAL VELOCITIES UBAR AND VBAR
KBHA=KRHO                TRANP128
KBHR=KRHC                TRANP129
IF(KAY.LT.0) GO TO 405      TRANP130
KBHA=KRHC                TRANP131
KBHR=KRHO                TRANP132
IF(KAY.LT.0) GO TO 405      TRANP133
KBHA=KRHC                TRANP134
405 CALL GETDA( USUM,ZBf,KBHA,KBHB,NDATO,LTIM, UBAR,KRHF,NDATF,LTIMF)  TRANP135
CALL GETDA( VSUM,ZBf,KBHA,KBHB,NDATO,LTIM, VBAR,KRHF,NDATF,LTIMF)  TRANP136
407 IF(NDEP.NE.0) GO TO 412      TRANP137
COMPUTE AVERAGE HORIZONTAL DISPERSION AND WIND ORIENTATION ANGLE
CALL GETDA(DXSUM,ZBf,KBHA,KBHB,NDATO,LTIM,DXBAR,KRHF,NDATF,LTIMF)  TRANP138
CALL GETDA(DYSUM,ZBf,KBHA,KBHB,NDATO,LTIM,DYBAR,KRHF,NDATF,LTIMF)  TRANP139
CALL GETDA( RSUM,ZBf,KBHA,KBHB,NDATO,LTIM, RBAR,KRHF,NDATF,LTIMF)  TRANP140
RC=R0+RBAR                TRANP141
SIGXC=SIGX0+DXBAR*TSEG    TRANP142
SIGYC=SIGY0+DYBAR*TSEG    TRANP143
COMPUTE CURRENT POSITION AND TIME (XC,YC,ZC,TC)
412 TC=T0+TSEG            TRANP144
ZC=Z0+WBAR*TSEG          TRANP145
XC=X0+UBAR*TSEG          TRANP146
YC=Y0+VBAR*TSEG          TRANP147
XC=X0+UBAR*TSEG          TRANP148
YC=Y0+VBAR*TSEG          TRANP149
CALL NEST(NET,NETSU,XC,YC,NDATC,XL,XR,YL,YU,ICF,JCF,NCF)  TRANP150
IF(MC(4).EQ.1) WPITE(ISOUT,3) TC,ZC,XC,YC,NDATC          TRANP151
COMPARE CURRENT MESH INDEX NDATC WITH PREVIOUS MESH INDEX NDATO
IF(NDATC.EQ.NDATO) GO TO 700          TRANP152
COMPUTE INTERPOLATED PGINT
XT=XC                      TRANP153
YT=YC                      TRANP154
ZT=ZC                      TRANP155
IF (NODE.EQ.0) GO TO 213      TRANP156
CALL BCUNINET,METSU,XT,YT,X0,Y0,XC,YC,ICF,JCF,NCF  TRANP157
ZC=SORT((XT-XC)**2+(YT-YC)**2)/((XT-X0)**2+(YT-Y0)**2)  TRANP158
ZC=ZT+ZC*(Z0-ZT)            TRANP159
IF(APS(WBAR).LE.1.0E-30) GO TO 510      TRANP160
TSEG=(ZC-Z0)/WBAR          TRANP161
GO TO 518                  TRANP162
510 IF(ABS(UBAR).LE.1.0E-30) GO TO 513      TRANP163
TSEG=(XC-X0)/UBAR          TRANP164
GO TO 518                  TRANP165
513 IF(ABS(VBAR).LE.1.0E-30) GO TO 516      TRANP166
TSEG=(YC-Y0)/VBAR          TRANP167
GO TO 518                  TRANP168
516 CALL ERROR(PRGGPM,516,ISOUT)  TRANP169
RETURN                     TRANP170
518 IF(NDEP.NE.0) GO TO 521      TRANP171
RC=R0+RBAR                TRANP172
TRANP173
TRANP174

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SIGXC=SIGX0+DXBAR*TSEG          TRANP175
SIGYC=SIGYO+DYBAR*TSEG          TRANP176
521  TC=T0+TSEG                  TRANP177
CALL NEST(NET,NETSU,XC,YC,NDATC,XL,XR,YL,YU,ICF,JCF,NCF) TRANP178
CHECK IF PARCEL CENTER POSITION IS OSCILLATING
IF ((KBH01.NE.KBH0).OR.(KBHC1.NE.KBHC).OR.(NDTC1.NE.NDATC).OR.
1(NDTO1.NE.NDATO)) GO TO 626    TRANP179
IF (MC(4).EQ.1) WRITE(15OUT,4) XP,YP,ZP,TB,XG,YC,ZC,TC      TRANP180
CALL CNTRINET,NETSU,NDATO,XG,YG,ICF,JCF,NCF1                 TRANP181
XQ=XG
YQ=YG
CALL NEST(NET,NETSU,XQ,YQ,NDATQ,XL,XR,YL,YU,ICF,JCF,NCF)  TRANP182
CLEAR STORED MESH AND STRATUM INDICES
NDTC1=0                         TRANP183
NDTO1=0                         TRANP184
KBHC1=0                         TRANP185
KBH01=0                         TRANP186
CHANNEL WAFER CENTER POSITION ALONG APPROPRIATE CELL BOUNDARY
SPE=2.*EPS                        TRANP187
IF ((ABS(XLO-XR).GT.SPE).AND.(ABS(XR0-XL).GT.SPE)) GO TO 616  TRANP188
UMAR=0,                            TRANP189
CALL GETDAE USUM,ZRF,KPH,KBHR,NDATO,LTIM,VRARC,KRHF,NDATF,LTIME) TRANP190
IF (ARS(UBARC).LE.ABS(VRARC)) GO TO 407                      TRANP191
VRAR=VRARC
NDATO=NDATC
GO TO 407
616  IF ((ABS(YLO-YU).GT.SPE).AND.(ABS(YU0-YL).GT.SPE))
1CALL ERROR(PROGP4,616,ISOUT)
VRAR=0.
CALL GETDAE USUM,ZRF,KPH,KBHR,NDATG,LTIM,UBARC,KRHF,NDATF,LEIMP) TRANP192
IF (ABS(UBARC).LE.ABS(VRARC)) GO TO 407                      TRANP193
UBAR=UBARC
NDATC=NDATG
GO TO 407
COMMIV PREVIOUS AND CURRENT MESH AND STRATUM INDICES TO STORAGE
626  NDTC1=NDATO                  TRANP194
NDTO1=NDTC1                  TRANP195
KBHC1=XPHC                  TRANP196
KBH01=KBH0                  TRANP197
CONVERT X0,YC,Z0,T0,SIGX0,SIGY0, AND NDATC TO CURRENT V-LUES
700  Z0=ZC                       TRANP198
X0=XC
Y0=YC
T0=TC
NDATO=NDATC
IF (MC(4).EQ.1) WRITE(15OUT,2) T0,ZC,X0,Y0,NDATO
IF (INDEP.NE.0) GO TO 709
SIGXC=SIGXC
SIGYO=SIGYO
RO=RC
CHECK IF CURRENT POSITION IS OUTSIDE ATMOSPHERE
708  IF (NDATO.LE.0) GO TO 710
IF (KRIP.EQ.1) GO TO 709
8  IF DEPOSITION PLANE IS REACHED OR TRANSPORT TIME LIMIT IS EXCEEDED TRANP228
9  EXIT FROM TRANP, OTHERWISE RETURN TO VCP
IF (( (T0-ZDEP).LE.EPS2).OR.(T0-IMSK-(G).LE.EPST)) GO TO 721  TRANP229
GO TO 100G
709  CONTINUE

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CHECK IF TOTAL FLIGHT TIME HAS BEEN EXHAUSTED  
 IF(TO+EPST-TDEP) 200,720,720  
 CARRY PARCEL CENTER BACK INTO ATMOS. IF NDEP IS NOT EQUAL TO ZERO  
 710 IF(NDEP.EQ.0) GO TO 720  
 XO=XO-2.\*EPS.  
 YO=YO-2.\*EPS  
 CALL NESTINET,NETSU,XO,YO,NDATO,XL,YR,YL,YU,ICF,JCF,NCF)  
 IF(NDATO.GT.0) GO TO 720  
 714 XO=XO+4.\*EPS  
 YO=YO+4.\*EPS  
 CALL NESTINET,NETSU,XO,YO,NDATO,XL,YR,YL,YU,ICF,JCF,NCF)  
 IF(NDATO.LE.0) CALL ERROR(PROGRAM,720,ISOUT)  
 COMPUTE HORIZ. DISPERSION IF NDEP IS NOT EQUAL TO ZERO  
 720 IF(NDEP.NE.0) RETURN  
 P2=PWAFF\*\*2  
 IF(MC(10).EQ.1) GO TO 721  
 SIGXC=2.\*DOWN\*SIGXC  
 SIGYC=2.\*CROSS\*SIGYC  
 GO TO 722  
 721 TRIP=TC-TP  
 DSPRTX=SIGX0/TRIP  
 TONEX=4.\*((R2/DSPRTX)\*\*(1./3.))  
 IF(TRIP.LE.TONEX) SIGX0=DSPRTX\*TONEX\*(TRIP\*\*2)/3.  
 IF(TRIP.GT.TONEX) SIGXC=DSPRTX\*(TRIP\*\*3)/3.  
 SIGX0=SIGX0\*(DOWN\*\*(.1./2.))  
 DSPRTY=SIGY0/TRIP  
 TONEY=4.\*((R2/DSPRTY)\*\*(1./3.))  
 IF(TRIP.LE.TONEY) SIGYC=DSPRTY\*TONEY\*(TRIP\*\*2)/3.  
 IF(TRIP.GT.TONEY) SIGYC=DSPRTY\*(TRIP\*\*3)/3.  
 SIGY0=SIGY0\*(CROSS\*\*(.1./2.))  
 722 SIGX0=SQR((R2+SIGX0))  
 SIGY0=SQR((R2+SIGY0))  
 RETURN  
 END

TRANP233  
 TRANP234  
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